# TJI® 110, TJ® 210, TJI 230, TJi 360, TJ® 560, AND TJI 560D JOISTS 



## Featuring Trus Joist ${ }^{\circledR}$ TJI ${ }^{\circledR}$ Joists for Floor and Roof Applications

- Uniform and Predictable
- Lightweight for Fast Installation
- Resource Efficient
- Resists Bowing, Twisting, and Shrinking
- Significantly Reduces Callbacks
- Available in Long Lengths
- Limited Product Warranty



The products in this guide are readily available through our nationwide network of distributors and dealers. For more information on other applications or other Trus Joist ${ }^{\circledR}$ products, contact your Weyerhaeuser representative.

This guide is for use with NBCC 2010, NBCC 2015, CSA 086-09, and CSA 086-14.

## Code Evaluations:

CCMC 13132-R, CCRR 0222C

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SUSTAINABLE FORESTRY initiative

## Why Choose Trus Joist ${ }^{\circledR}$ TJI ${ }^{\circledR}$ Joists?

- Engineered for strength and consistency
- Efficient installation saves time and labor
- Longer lengths allow more versatile floor plans
- Less jobsite waste
- Fewer red tags and callbacks


Now more than ever builders need solutions that really deliver. That's why Trus Joist ${ }^{\circledR}$ TJI® joists are designed to give you more-longer lengths, easier installation, higher span values, better strength-to-weight ratios, and faster cycle times.
$\mathrm{T} \|^{\circledR}$ joists are also available in deeper depths that are suitable for heavier-duty loads, such as those in multi-family structures and light commercial buildings.

## This guide features $T J{ }^{\circledR}$ joists in the following sizes:

Depths: $9^{1 ⁄ 2} 2^{\prime \prime}, 11$ ¹/8", 14 ", 16 ", 18 ", 20 ", 22", and 24 "
Flange Widths: $13 / 4^{\prime \prime}, 2 \frac{1}{16} 6^{\prime \prime}, 25 / 16^{\prime \prime}$, and $31 / 2^{\prime \prime}$
Flange height and thickness vary by series; see the appropriate sections of this guide for specific sizes and relevant technical information:

## 91/2"-16" Section 1:

JOISTS Design information for $911 / 2$ " -16 " $\mathrm{TJI}{ }^{\circledR}$ joists

## 18"-24"

## Section 2:

JOISTS Design information for 18"- 24" TJI® joists

## ALL JOIST Section 3:

DEPTHS Framing details and design information for all joist depths in this guide

> Some products may not be available in your region.
> Contact your Weyerhaeuser representative at our Specification Center or visit "Where to Buy".

Safety data sheets for all Weyerhaeuser wood products can be found on our website at: weyerhaeuser.com/sustainability/environment/product-stewardship/safety-data-sheets.

PRODUCT STORAGE


CAUTION:
Wrap is slippery when wet or icy

Align stickers (2x3 or larger) directly over support blocks

Use support blocks (6x6 or larger) at 10' on-centre to keep bundles out of mud and water

Certified Sourcing
www.sfiprogram.org SF-00008

For over 40 years, prefabricated wood I-joists and other Weyerhaeuser building products have established a record of safe and reliable performance in millions of structures. Many of these structures, such as one- or two-family residential dwellings, do not require specific fire-resistance ratings per building codes but may require unrated membrane protection. The information below is intended to help you specify and install Trus Joist ${ }^{\circledR}$ products with fire safety in mind.

## One-Hour Assembly for Rated Construction

## Double Layer



## Suggested Minimum Membrane Protection for Unrated Construction

1. Appropriate span-rated sheathing (Exposure 1).
2. $\mathrm{TJI}{ }^{\circledR}$ joist
3. Single-layer of $1 / 2$ " gypsum board

4. Two layers of $5 / 8$ " Type $X$ gypsum board complying with ASTM C1396 or two layers of $1 / 2$ " Type C gypsum board.
5. $\mathrm{TJI}{ }^{\circledR}$ joist
6. $31 / 2$ "-thick glass fiber insulation (optional)
7. Resilient channels (required if insulation is used, optional if insulation is omitted)

Intertek listings:
WNR FCA 60-01 (no channels)
WNR FCA 60-03 (with channels)

For more information on fire assemblies and fire-safe construction, please refer to the Weyerhaeuser Fire-Rated Assemblies and Sprinkler Systems Guide, TJ-1500, or visit weyerhaeuser.com/woodproducts.

## TIPS FOR PREVENTING FLOOR NOISE

Trus Joist ${ }^{\circledR}$ TJI® joists are structurally uniform and dimensionally stable, and they resist shrinking and twisting. This helps prevent gaps from forming around the nails between the joist and the floor panels-gaps that can potentially cause squeaks or other floor noise. Using TJ® joists can help you build a quieter floor, but only if the entire floor system is installed properly. This is because other components of the floor system, such as hangers, connectors, and nails can be a source of floor noise.

Properly Seat Each Joist in Hanger


Seat the joist tight to the bottom of the hanger. When using hangers with tabs, bend the flange tabs over and nail to the TJI® joist bottom flange. Placing a dab of sublfoor adhesive* in the seat of the hanger prior to installing the joist can reduce squeaks.

## Use Adhesive and Special Nailing When Needed



Nail interior partitions to the joists when possible. If the wall can be nailed only to the floor panel, run a bead of adhesive* under the wall and either cross nail, nail through and clinch tight, or screw tightly into the wall from below.


Keep building materials dry, and properly glue floor panels to the joists. Panels that become excessively wet during construction shrink as they dry. This shrinkage may leave gaps that allow the panel to move when stepped on.

## Avoid "Shiners"



Exercise care when nailing. Nails that barely hit the joists (shiners) do not hold the panel tight to the joist and should be removed. If left in, the nails will rub against the side of the joist when the panel deflects.

[^0]For more information and tips on how to prevent floor noise, refer to the Weyerhaeuser Prevention and Repair of Floor System Squeaks Technical Resource Sheet, 9009, or contact your Weyerhaeuser representative.


Some products may not be available in your region.
Contact your Weyerhaeuser representative at our Specification Center or visit "Where to Buy".

## TJ-PRO™ RATING AND FLOOR PERFORMANCE

## What is Floor Performance and TJ-Pro Rating?

Floor performance is how a floor feels under foot traffic. TJ-Pro Rating is a diagnostic tool developed by Weyerhaeuser to help you assess floor performance based on the floor assembly components you specify. You can access TJ-Pro rating using our ForteWEB ${ }^{\text {TM }}$ and Javelin ${ }^{\text {® }}$ software platforms or our span table web app.

## How does TJ-Pro Rating Work?

Point values up to 65 are assigned using complex algorithms based on field and laboratory research conducted on over 600 floor system assemblies. It also factors in the variables listed under Key
Factors Affecting
Performance shown to the right. Ranges can then be correlated to
 customer floor performance expectations.

## What do the ratings mean?

The ratings represent the percentage of customers that would be satisfied with the floor performance. At 45 points, customer satisfaction is $84 \%$. At 65 points, it's nearly $100 \%$.

## How can you use TJ-Pro Rating?

You know your market and TJ-Pro Ratings let you build what your market needs. For example, once you know that a TJ-Pro Rating of 45 points works for your customers, you can simply target 45 points for your other floors to deliver the performance your market expects.

It's also a great tool to optimize floors for the type of home you build:
Entry Level: Focus on economy and efficiency. Use TJ-Pro Ratings to make sure you're not overbuilding.

Move-Up/Mid-Level: Countless floor plans with upgrades options. Use TJ-Pro Rating to consistently and reliably build across the range of framing solutions.

High-End Luxury: Uncompromised quality and reputation is key. From our experience, homeowners in this group expect a rating of 45 points or greater. Use TJ-Pro Rating to differentiate yourself and deliver the quality your customers demand.

## Key Factors Affecting Performance

- Basic Stiffness is a combination of joist depths and span.
- Composite Action-Careful nailing in conjunction with construction adhesives increases basic stiffness.
- Continuity-Continuous joists over several supports generally perform better than simple spans. Care must be taken if the joists continue into another occupancy.
- Joist Spacing and Deck StiffnessReduced spacing or increased deck thickness generally improves floor performance.
- Ceilings directly applied to the bottom edge of the floor members, or equivalent 1 x or 2 x strapping, is a performance enhancement.
- Beams-Floor systems supported by steel or wood beams tend to feel less stiff than those supported by solid bearing walls.
- Bridging or Blocking can be a contributor to improved floor performance.
- Non-bearing Partition Walls dampen vibration and improve floor performance when installed transverse to the floor joists.
- Mass reduces damping in a floor system causing a decrease in floor performance. This impact is more noticeable as span lengths increase.

TJ-Pro Rating is featured in these design software platforms.


Autodesk ${ }^{\circledR}$ Revit ${ }^{\circledR}$ linked to ForteWEB ${ }^{\text {TM }}$

[^1]This section contains design information for $9 \underline{1} / 2^{\prime \prime}-16$ deep Trus Joist ${ }^{\circledR}$ TJ ${ }^{\circledR}$ joists.
These standard-size $\mathrm{TJ}^{\circledR}$ joists are readily available through your local Weyerhaeuser dealer or distributor. Offered with the flange sizes shown below, they come in lengths up to 60' (in 1' increments).

## Design Properties

| Depth | TJ ${ }^{\text {® }}$ | Joist Weight (lbs/ft) | Joist Only El x $10^{6}$ (lbs-in. ${ }^{2}$ ) | Factored Resistances-Standard Term |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Maximum Resistive Moment ${ }^{(1)}$ (ft-lbs) | Maximum Vertical Shear (lbs) | 13/4" End Reaction (lbs) |  | 3½" Intermediate Reaction (lbs) |  | 514" Intermediate Reaction (lbs) |  |
|  |  |  |  |  |  | No Web Stiffeners | With Web Stiffeners | No Web Stiffeners | With Web Stiffeners ${ }^{(2)}$ | No Web Stiffeners | With Web <br> Stiffeners |
|  | 110 | 2.3 | 157 | 4,160 | 1,925 | 1,435 | N.A. | 3,055 | N.A. | 3,705 | N.A. |
|  | 210 | 2.6 | 186 | 4,990 | 2,100 | 1,585 | N.A. | 3,385 | N.A. | 4,050 | N.A. |
| 91/2" | 230 | 2.7 | 206 | 5,540 | 2,100 | 1,675 | N.A. | 3,800 | N.A. | 4,405 | N.A. |
|  | 360 | 2.7 | 249 | 7,965 | 2,250 | 1,705 | N.A. | 3,885 | N.A. | 4,740 | N.A. |
|  | 560 | 3.6 | 378 | 12,235 | 2,635 | 1,995 | N.A. | 4,735 | N.A. | 5,455 | N.A. |
|  | 110 | 2.5 | 267 | 5,255 | 2,460 | 1,435 | 1,885 | 3,055 | 3,575 | 3,705 | 4,225 |
|  | 210 | 2.8 | 315 | 6,310 | 2,610 | 1,585 | 2,105 | 3,385 | 3,905 | 4,050 | 4,570 |
| 117/8" | 230 | 3.0 | 347 | 7,010 | 2,610 | 1,675 | 2,190 | 3,800 | 4,320 | 4,405 | 4,925 |
|  | 360 | 3.0 | 419 | 10,280 | 2,690 | 1,705 | 2,225 | 3,885 | 4,400 | 4,740 | 5,255 |
|  | 560 | 4.0 | 636 | 15,795 | 3,235 | 1,995 | 2,680 | 4,735 | 5,425 | 5,455 | 6,140 |
|  | 110 | 2.8 | 392 | 6,220 | 2,935 | 1,435 | 1,885 | 3,055 | 3,575 | 3,705 | 4,225 |
|  | 210 | 3.1 | 462 | 7,470 | 3,070 | 1,585 | 2,105 | 3,385 | 3,905 | 4,050 | 4,570 |
| 14" | 230 | 3.3 | 509 | 8,300 | 3,070 | 1,675 | 2,190 | 3,800 | 4,320 | 4,405 | 4,925 |
|  | 360 | 3.3 | 612 | 12,200 | 3,085 | 1,705 | 2,225 | 3,885 | 4,400 | 4,740 | 5,255 |
|  | 560 | 4.2 | 926 | 18,755 | 3,770 | 1,995 | 2,680 | 4,735 | 5,425 | 5,455 | 6,140 |
|  | 210 | 3.3 | 629 | 8,550 | 3,455 | 1,585 | 2,105 | 3,385 | 3,905 | 4,050 | 4,570 |
| 16" | 230 | 3.5 | 691 | 9,495 | 3,455 | 1,675 | 2,190 | 3,800 | 4,320 | 4,405 | 4,925 |
| 16 | 360 | 3.5 | 830 | 13,980 | 3,455 | 1,705 | 2,225 | 3,885 | 4,400 | 4,740 | 5,255 |
|  | 560 | 4.5 | 1,252 | 21,495 | 4,280 | 1,995 | 2,680 | 4,735 | 5,425 | 5,455 | 6,140 |

(1) Caution: Do not increase joist moment design properties by a repetitive-member-use factor.
(2) See detail $W$ on page 28 for web stiffener requirements and nailing information.

## General Notes

- Factored resistances are based on Limit States Design per CSA 086.
- Factored reaction includes all loads on the joist.
- Factored shear is computed at the inside face of supports and includes all loads on the span(s). Factored shear resistance may sometimes be increased at interior supports. For more information contact your Weyerhaeuser representative.
- The following formulas approximate the simple span uniform load deflection of $\Delta$ (inches):

For TJI® 110, 210, 230, and 360 Joists

## For TJI® 560 Joists

$$
\Delta=\frac{22.5 \mathrm{wL}^{4}}{\mathrm{El}}+\frac{2.67 \mathrm{wL}^{2}}{\mathrm{dx1} 0^{5}}
$$

$$
\Delta=\frac{22.5 \mathrm{wL}^{4}}{\mathrm{El}}+\frac{2.29 \mathrm{wL}^{2}}{\mathrm{~d} \times 10^{5}}
$$

$w=$ uniform load in pounds per linear foot
d $=$ out-to-out depth of the joist in inches
$L=$ span in feet
$\mathrm{El}=$ value from table above


TJI® 110 joists


TJI® 210 joists


TJI® 230 joists


TJI® 360 joists


TJI® 560 joists


DO NOT walk on joists until braced. INJURY MAY RESULT.

## DO NOT stack

 building materials on unsheathed joists. Stack only over beams or walls.DO NOT walk on joists that are lying flat.

## WARNING

Joists are unstable until braced laterally

Bracing Includes: - Blocking - Hangers - Rim Board - Sheathing - Rim Joist - Strut Lines

WARNING NOTES:
Lack of proper bracing during construction can result in serious accidents. Observe the following guidelines:

1. All blocking, hangers, rim boards, and rim joists at the end supports of the $T J \|^{\circledR}$ joists must be completely installed and properly nailed.
2. Lateral strength, like a braced end wall or an existing deck, must be established at the ends of the bay. This can also be accomplished by a temporary or permanent deck (sheathing) fastened to the first 4 feet of joists at the end of the bay.
3. Safety bracing of $1 \times 4$ (minimum) must be nailed to a braced end wall or sheathed area (as in note 2) and to each joist. Without this bracing, buckling sideways or rollover is highly probable under light construction loads-such as a worker or one layer of unnailed sheathing.
4. Sheathing must be completely attached to each $T J \|^{\circledR}$ joist before additional loads can be placed on the system.
5. Ends of cantilevers require safety bracing on both the top and bottom flanges.
6. The flanges must remain straight within a tolerance of $1 / 2^{\prime \prime}$ from true alignment.

5/8" OSB Subfloor (Glue-nailed)—Vibration-Controlled, Standard Term

| Depth | TJI ${ }^{\text {® }}$ | Directly Applied Ceiling |  |  |  |  |  | No Directly Applied Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Simple or Continuous Span |  |  | Continuous Span Only |  |  | Simple or Continuous Span |  |  | Continuous Span Only |  |  |
|  |  | 12" o.c. | 16" o.c. | 19.2" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. |
| 40 PSF Live Load / 15 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91/2" | 110 | 15'-9' | 14'-10" | 14'-4" | 16'-5' | 15'-6' | 15'-0" | 15'-3' | 14'-5" | 13'-11" | 15'-11" | 15'-0" | 14'-6" |
|  | 210 | 16'-1' | 15'-3' | 14'-8' | 16'-10" | 15'-11" | 15'-4" | 15'-8' | 14'-9" | 14'-3" | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-5" | 14'-11" |
|  | 230 | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-5" | 14'-11' | 17'-1' | $16^{\prime}-2^{\prime \prime}$ | 15'-7" | 15'-11' | 15'-0' | 14'-6" | 16'-8' | 15'-8' | 15'-2" |
|  | 360 | 16'-10' | 15'-11" | 15'-4' | 17'-7' | $16^{\prime}-7{ }^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | 16'-5' | $15^{\prime}-6^{\prime \prime}$ | 14'-11" | 17'-2' | $16^{\prime}-2{ }^{\prime \prime}$ | 15'-8' |
|  | 560 | 18'-2' | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-5^{\prime \prime}$ | 19'-2' | 17'-10" | $17^{\prime}-2{ }^{\prime \prime}$ | 17'-9" | $16^{\prime}-8^{\prime \prime}$ | $16^{\prime}-1{ }^{\prime \prime}$ | $18^{\prime}-8^{\prime \prime}$ | 17'-5' | 16'-10' |
| 111/8" | 110 | 17'-7' | 16'-8' | $16^{\prime}-1^{\prime \prime}$ | 18'-7' | 17'-5" | $16^{\prime}-10^{\prime \prime}$ | 17'-1' | $16^{\prime}-1{ }^{\prime \prime}$ | $15^{\prime}-7{ }^{\prime \prime}$ | 17'-10' | $16^{\prime}-10^{\prime \prime}$ | 16'-3' |
|  | 210 | 18'-1' | 17'-1' | $16^{\prime}-6^{\prime \prime}$ | 19'-2' | 17'-10" | $17^{\prime}-3^{\prime \prime}$ | 17'-7' | $16^{\prime}-6^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | 18'-5' | 17'-3' | $16^{\prime}-8^{\prime \prime}$ |
|  | 230 | 18'-5' | 17'-4' | $16^{\prime}-9{ }^{\prime \prime}$ | 19'-6' | 18'-2' | 17'-6' | 17'-10" | 16'-10' | $16^{\prime}-3^{\prime \prime}$ | 18'-10' | 17'-7' | $16^{\prime}-11^{\prime \prime}$ |
|  | 360 | 19'-2' | 17'-10" | 17'-2' | 20'-3' | 18'-10" | 18'-0' | 18'-6" | 17'-4' | 16'-9' | 19'-7' | 18'-2' | 17'-6' |
|  | 560 | 21'-0' | 19'-5' | 18'-6" | 22'-2' | 20'-6" | 19'-7' | 20'-5' | 18'-10" | 18'-0' | 21'-7" | 19'-11" | 19'-1' |
| $14 "$ | 110 | 19'-6' | 18'-2' | 17'-6' | 20'-8' | 19'-3' | 18'-5' | 18'-9' | 17'-6' | 16'-11' | 19'-9'' | 18'-4' | 17'-8' |
|  | 210 | $20^{\prime}-2^{\prime \prime}$ | 18'-9'' | 17'-11' | 21'-3' | 19'-10" | 19'-0' | 19'-5' | $18^{\prime}-0^{\prime \prime}$ | 17'-4' | 20'-6' | 19'-0' | 18'-2' |
|  | 230 | 20'-6" | 19'-1" | 18'-3' | 21'-8' | 20'-2' | 19'-4' | 19'-9' | $18^{\prime}-4^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | 20'-11' | 19'-5' | 18'-7" |
|  | 360 | 21'-3' | 19'-9'' | 18'-10" | $22^{\prime}-6^{\prime \prime}$ | 20'-11' | 20'-0' | 20'-7' | 19'-1' | 18'-3' | 21'-9" | 20'-2' | 19'-3' |
|  | 560 | 23'-4' | 21'-7' | 20'-7' | 24'-8" | 22'-10' | 21'-9' | 22'-8' | 20'-11" | $20^{\prime}-0^{\prime \prime}$ | 24'-0' | 22'-2' | 21'-2' |
| 16" | 210 | 21'-11" | 20'-5' | 19'-6' | 23'-2' | 21'-7" | 20'-8' | 21'-1' | 19'-7' | 18'-9' | 22'-4" | 20'-8' | 19'-9' |
|  | 230 | 22'-4' | 20'-9' | 19'-10" | 23'-8' | $22^{\prime}-0^{\prime \prime}$ | 21'-0' | 21'-6" | 19'-11" | 19'-1' | 22'-9" | 21'-1' | 20'-2' |
|  | 360 | $23^{\prime}-2^{\prime \prime}$ | $21^{\prime}-6^{\prime \prime}$ | 20'-7' | $24^{\prime}-6{ }^{\prime \prime}$ | 22'-9' | 21'-9' | $22^{\prime}-5^{\prime \prime}$ | 20'-9' | 19'-10" | $23^{\prime}-8^{\prime \prime}$ | 21'-11" | 20'-11" |
|  | 560 | 25'-5' | 23'-6' | 22'-5' | 26'-10' | 24'-10" | 23'-8' | 24'-8' | 22'-9' | 21'-9" | 26'-2' | 24'-1" | 23'-0' |
| 40 PSF Live Load/30 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91/2" | 110 | 15'-9' | 14'-10" | 14'-4" | 16'-5' | 15'-6" | 14'-6" | 15'-3' | 14'-5" | 13'-11" | 15'-11" | 15'0" | 14'-6" |
|  | 210 | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-3' | 14'-8' | 16'-10' | 15'-11" | 15'-4" | 15'-8' | 14'-9" | 14'-3" | $16^{\prime}-4^{\prime \prime}$ | 15'-5" | 14'-11" |
|  | 230 | $16^{\prime}-4^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | 14'-11" | 17'-1' | $16^{\prime}-2^{\prime \prime}$ | 15'-7' | 15'-11' | $15^{\prime}-0^{\prime \prime}$ | $14^{\prime}-6^{\prime \prime}$ | $16^{\prime}-8^{\prime \prime}$ | $15^{\prime}-8^{\prime \prime}$ | $15^{\prime}-2^{\prime \prime}$ |
|  | 360 | 16'-10' | 15'-11" | 15'-4" | 17'-7" | $16^{\prime}-7{ }^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | 16'-5' | 15'-6" | 14'-11" | 17'-2' | $16^{\prime}-2{ }^{\prime \prime}$ | 15'-8" |
|  | 560 | 18'-2' | 17'-0' | $16^{\prime}-5^{\prime \prime}$ | 19'-2' | 17'-10" | 17'-2" | 17'-9' | $16^{\prime}-8^{\prime \prime}$ | $16^{\prime}-1^{\prime \prime}$ | 18'-8' | 17'-5' | $16^{\prime}-10^{\prime \prime}$ |
| 117/8" | 110 | 17'-7' | $16^{\prime}-8^{\prime \prime}$ | 16'-1'(1) | 18'-7" | 17'-5' | $16^{\prime}-2^{\prime \prime}(1)$ | 17'-1' | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-7'(1) | 17'-10" | 16'-10" | $16^{\prime}-3^{\prime \prime}(1)$ |
|  | 210 | 18'-1' | 17'-1" | $16^{\prime}-6^{\prime \prime}$ | 19'-2' | 17'-10" | $17^{\prime}-3^{\prime \prime}(1)$ | 17'-7" | $16^{\prime}-6^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | $18^{\prime}-5^{\prime \prime}$ | 17'-3' | $16^{\prime}-8^{\prime \prime}$ |
|  | 230 | $18^{\prime}-5^{\prime \prime}$ | 17'-4' | 16'-9' | 19'-6' | 18'-2' | $17^{\prime}-6^{\prime \prime}$ | 17'-10" | $16^{\prime}-10^{\prime \prime}$ | $16^{\prime}-3^{\prime \prime}$ | 18'-10' | 17'-7' | $16^{\prime}-11^{\prime \prime}$ |
|  | 360 | 19'-2' | 17'-10" | 17'-2' | 20'-3' | 18'-10" | 18'-0' | 18'-6' | 17'-4' | $16^{\prime}-9{ }^{\prime \prime}$ | 19'-7' | 18'-2' | $17^{\prime}-6^{\prime \prime}$ |
|  | 560 | $21^{\prime}-0^{\prime \prime}$ | 19'-5' | 18'-6" | $22^{\prime}-2^{\prime \prime}$ | $20^{\prime}-6^{\prime \prime}$ | 19'-7' | 20'-5' | $18^{\prime}-10^{\prime \prime}$ | $18^{\prime}-0^{\prime \prime}$ | 21'-7" | 19'-11' | 19'-1' |
| 14" | 110 | 19'-6' | 18'-2' | $17^{\prime}-6^{\prime \prime}(1)$ | 20'-8' | 19'-3"(1) | 17'-9"(1) | 18'-9' | 17'-6" | $16^{\prime}-11^{1 \prime}(1)$ | 19'-9'' | 18'-4' | 17'-8'(1) |
|  | 210 | 20'-2' | 18'-9' | 17'-11'(1) | 21'-3' | 19'-10' | $19^{\prime}-0^{\prime \prime \prime}(1)$ | 19'-5' | $18^{\prime}-0^{\prime \prime}$ | $17^{\prime}-4^{\prime \prime}(1)$ | $20^{\prime}-6^{\prime \prime}$ | 19'-0' | $18^{\prime}-2^{1 \prime}(1)$ |
|  | 230 | 20'-6" | 19'-1" | 18'-3' | $21^{\prime}-8^{\prime \prime}$ | $20^{\prime}-2$ " | 19'-4' | 19'-9'' | 18'-4' | $17^{\prime}-8^{\prime \prime}$ | 20'-11" | 19'-5" | 18'-7" |
|  | 360 | $21^{\prime}-3^{\prime \prime}$ | 19'-9" | 18'-10'1 | 22'-6" | 20'-11' | $20^{\prime}-0^{\prime \prime}(1)$ | 20'-7' | 19'-1" | 18'-3' | 21'-9" | 20'-2" | 19'-3' |
|  | 560 | 23'-4' | 21'-7" | 20'-7' | 24'-8' | 22'-10" | 21'-9" | 22'-8" | 20'-11' | 20'-0' | 24'-0" | 22'-2' | 21'-2' |
| $16^{\prime \prime}$ | 210 | 21'-11" | $20^{\prime}-5^{\prime \prime}$ | $19^{\prime}-6^{\prime \prime \prime}(1)$ | $23^{\prime}-2{ }^{\prime \prime}$ | $21^{\prime}-7^{\prime \prime}(1)$ | 19'-11'(1) | 21-1' | 19'-7" | 18'-9'(1) | 22'-4" | $20^{\prime}-8{ }^{\prime \prime}$ | 19'-9'(1) |
|  | 230 | $22^{\prime}-4{ }^{\prime \prime}$ | 20'-9' | 19'-10'(1) | 23'-8' | 22'-0' | $21^{\prime}-0^{\prime \prime}(1)$ | 21'-6' | 19'-11" | 19'-1' | 22'-9' | 21'-1' | 20'-2'(1) |
|  | 360 | $23^{\prime}-2^{\prime \prime}$ | $21^{\prime}-6^{\prime \prime}$ | 20'-7'1(1) | $24^{\prime}-6{ }^{\prime \prime}$ | 22'-9" | 21'-9'(1) | $22^{\prime}-5^{\prime \prime}$ | 20'-9' | 19'-10'(1) | $23^{\prime}-8^{\prime \prime}$ | 21'-11" | 20'-11"(1) |
|  | 560 | 25'-5' | $23^{\prime}-6^{\prime \prime}$ | 22'-5' | $26^{\prime}-10^{\prime \prime}$ | 24'-10" | 23'-8' | $24^{\prime}-8^{\prime \prime}$ | 22'-9" | 21'-9" | 26'-2' | $24^{\prime}-1{ }^{\prime \prime}$ | 23'-0'1 |

(1) Web stiffeners are required at intermediate supports of continuous-span joists when the intermediate bearing length is less than $5 \frac{1}{4}$ " and the span on either side of the intermediate bearing is greater than the following spans:

| 40 PSF Live Load / 15 PSF Dead Load |  |  |  | 40 PSF Live Load / 30 PSF Dead Load |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TJI® | 12" o.c. | 16" o.c. | 19.2" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. |
| 110 | Not Required |  |  | Not Required | 18'-8" | 15'-6" |
| 210 |  |  |  | 20'-8" | 17'-3" |
| 230 |  |  |  |  | 19'-4" |
| 360 |  |  |  |  | 19'-9" |
| 560 |  |  |  |  |  |

- Bold italic spans indicate floors that would meet National Building Code of Canada (NBCC) vibration criteria but would be considered by 35\% of the population to have marginal or unacceptable performance.


## How to Use These Tables

1. Determine the subflooring thickness and applicable live and dead loads.
2. Determine whether the ceiling will be directly applied and what the span condition is (simple or continuous)
3. Select on-centre spacing.
4. Scan down the column until you meet or exceed the span of your application.
5. Select TJI® joist and depth.

## See page 8 for General Notes.

3/4" OSB Subfloor (Glue-nailed)—Vibration-Controlled, Standard Term

| Depth | TJ ${ }^{\text {® }}$ | Directly Applied Ceiling |  |  |  |  |  |  |  | No Directly Applied Ceiling |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Simple or Continuous Span |  |  |  | Continuous Span Only |  |  |  | Simple or Continuous Span |  |  |  | Continuous Span Only |  |  |  |
|  |  | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 40 PSF Live Load / 15 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91/2" | 110 | 16'-6' | 15'-7" | 14'-10" | 13'-8' | 17'-3' | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-9" | 14'-5" | 16'-1' | 15'-2" | 14'-7" | 13'-8" | 16'-9' | 15'-10" | 15'-3" | 14'-5' |
|  | 210 | 16'-11' | 16'-0' | 15'-5' | 14'-5" | 17'-8" | 16'-9' | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-6" | 16'-6' | 15'-7' | $15 '-0^{\prime \prime}$ | 14'-5" | 17'-3' | 16'-3" | 15'-8" | 15'-0" |
|  | 230 | 17'-2' | $16^{\prime}-3^{\prime \prime}$ | 15'-8' | 14'-11" | 18'-0' | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-8' | 16'-9'' | 15'-10" | 15'-3' | 14'-7" | 17'-6' | 16'-6' | 15'-11" | 15'-3" |
|  | 360 | 17'-8' | $16^{\prime}-8^{\prime \prime}$ | $16^{\prime}-1{ }^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | 18'-8' | $17^{\prime}-5^{\prime \prime}$ | $16^{\prime}-10^{\prime \prime}$ | 16'-1" | $17^{\prime}-4{ }^{\prime \prime}$ | $16^{\prime}-4^{\prime \prime}$ | 15'-8' | 15'-1" | 18'-2' | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-5^{\prime \prime}$ | 15'-9'1 |
|  | 560 | 19'-3' | 17'-10" | 17'-2' | $16^{\prime}-5^{\prime \prime}$ | 20'-5' | 18'-11' | $18^{\prime}-0^{\prime \prime}$ | 17'-2' | 18'-10' | $17^{\prime}-6^{\prime \prime}$ | $16^{\prime}-10^{\prime \prime}$ | $16^{\prime}-2^{\prime \prime}$ | 19'-11" | $18^{\prime}-5^{\prime \prime}$ | $17^{\prime}-8^{\prime \prime}$ | 16'-11' |
| 117/8" | 110 | 18'-8' | 17'-6" | 16'-10" | 16'-2"(1) | 19'-9' | 18'-5' | 17'-8' | $16^{\prime}-2^{\prime \prime}(1)$ | 18'-0' | 16'-11" | $16^{\prime}-4{ }^{\prime \prime}$ | $15^{\prime}-8^{\prime \prime}(1)$ | 19'-0' | 17'-8' | 17'-1' | $16^{\prime}-2^{\prime \prime \prime}(1)$ |
|  | 210 | 19'-3' | 17'-11" | 17'-3' | $16^{\prime}-7{ }^{\prime \prime}$ | 20'-4' | 18'-11' | $18^{\prime}-1{ }^{\prime \prime}$ | 17'-4'1(1) | 18'-8' | $17^{\prime}-5^{\prime \prime}$ | $16^{\prime}-9{ }^{\prime \prime}$ | $16^{\prime}-1{ }^{\prime \prime}$ | 19'-8' | 18'-3' | $17^{\prime}-6^{\prime \prime}$ | 16'-10" |
|  | 230 | 19'-7'' | 18'-3' | 17'-6" | $16^{\prime}-9{ }^{\prime \prime}$ | 20'-9' | 19'-3" | 18'-5' | 17'-7" | 19'-0" | $17^{\prime}-8^{\prime \prime}$ | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-4{ }^{\prime \prime}$ | 20'-1' | 18'-7'' | 17'-9" | 17'-1" |
|  | 360 | 20'-4' | 18'-11' | 18'-0' | 17'-3' | 21'-6" | 20'-0' | 19'-1' | $18^{\prime}-1{ }^{\prime \prime}$ | 19'-9" | 18'-4" | 17'-7" | 16'-10'' | 20'-11" | 19'-4' | $18^{\prime}-5^{\prime \prime}$ | 17'-7" |
|  | 560 | 22'-3" | 20'-7' | 19'-7' | 18'-7' | 23'-7' | 21'-10" | 20'-9' | 19'-8' | 21'-9" | 20'-1' | 19'-2' | 18'-1' | 23'-0" | 21'-3'' | 20'-3' | 19'-2'' |
| $14 "$ | 110 | 20'-9" | 19'-4" | 18'-6" | 17'-7'(1) | 21'-11" | 20'-5' | 19'-6'(1) | 17'-8'(1) | 20'-0' | 18'-7" | 17'-9' | $17^{\prime}-0^{\prime \prime}(1)$ | 21'-1' | 19'-7" | 18'-8' | 17'-8'(1) |
|  | 210 | 21'-5' | 19'-11' | 19'-0' | 18'-0'(1) | 22'-8' | 21'-1' | 20'-1' | 19'-1'(1) | 20'-8' | 19'-2" | 18'-3' | 17'-6'1(1) | 21'-10" | 20'-3" | 19'-4' | $18^{\prime}-4^{\prime \prime}(1)$ |
|  | 230 | 21'-10" | 20'-3' | 19'-4' | 18'-4' | $23^{\prime}-1{ }^{\prime \prime}$ | 21'-5' | 20'-6' | 19'-5"(1) | 21'-1" | 19'-7" | $18^{\prime}-8^{\prime \prime}$ | 17'-9' | $22^{\prime}-4^{\prime \prime}$ | 20'-8' | 19'-8' | 18'-8' |
|  | 360 | 22'-7' | 21'-0' | 20'-0' | 18'-11" | 23'-11" | 22'-2' | 21'-2' | 20'-1'(1) | 22'-0" | 20'-4' | 19'-4' | 18'-4' | 23'-2' | 21'-6" | 20'-6' | 19'-5' |
|  | 560 | 24'-9'' | 22'-11" | 21'-9" | 20'-7' | 26'-2' | 24'-3" | 23'-1' | 21'-10'1 | 24'-2" | $22^{\prime}-4{ }^{\prime \prime}$ | 21'-3' | 20'-1' | 25'-7' | 23'-7' | 22'-5' | 21'-2' |
| 16" | 210 | 23'-4" | 21'-8" | 20'-9' | 19'-8'(1) | 24'-8' | 22'-11" | 21'-11'(1) | 19'-8'(1) | 22'-6" | 20'-10' | 19'-11' | 18'-10'(1) | 23'-9' | 22'-1' | 21'-0" | 19'-8'(1) |
|  | 230 | 23'-9" | 22'-1' | 21'-1' | $20^{\prime}-0^{\prime \prime \prime}(1)$ | 25'-1' | 23'-4' | 22'-3' | 21'-2'(1) | 23'-0' | 21'-3' | 20'-3' | 19'-3'1(1) | 24'-3' | 22'-6" | 21'-5' | $20^{\prime}-4^{\prime \prime}(1)$ |
|  | 360 | 24'-7' | 22'-10' | 21'-9" | 20'-8'(1) | $26^{\prime}-0^{\prime \prime}$ | 24'-2' | 23'-1' | 21'-10'(1) | 23'-11" | 22'-1' | 21'-1' | 19'-11'(1) | 25'-3' | 23'-4" | 22'-3' | 21-1"11) |
|  | 560 | 26'-11' | 24'-11" | 23'-9" | 22'-5' | 28'-6' | 26'-4' | 25'-1' | 23'-9' | 26'-4' | 24'-3' | 23'-1' | 21'-9' | 27'-10" | 25'-8" | 24'-5' | 23'-1' |
| 40 PSF Live Load / 30 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91/2" | 110 | 16'-6' | $15^{\prime}-7{ }^{\prime \prime}$ | $14^{\prime}-6^{\prime \prime}$ | 12'-5' | $17^{\prime}-3^{\prime \prime}$ | 15'-10' | $14^{\prime}-6^{\prime \prime}$ | 12'-5' | $16^{\prime}-1{ }^{\prime \prime}$ | 15'-2" | 14'-6" | 12-5 | 16'-9' | 15'-10" | 14'-6" | 12'-5' |
|  | 210 | 16'-11' | $16^{\prime}-0^{\prime \prime}$ | 15'-5' | 13'-9' | 17'-8' | 16'-9' | 15'-10" | 13'-9' | $16^{\prime}-6{ }^{\prime \prime}$ | 15'-7' | 15'-0" | 13'-9'' | 17'-3' | 16'-3" | 15'-8" | 13'-9' |
|  | 230 | $17^{\prime}-2^{\prime \prime}$ | 16'-3' | 15'-8' | 14'-11" | 18'-0' | 17'-0' | $16^{\prime}-4{ }^{\prime \prime}$ | 14'-11" | 16'-9'' | 15'-10" | 15'-3" | 14'-7" | $17^{\prime}-6^{\prime \prime}$ | $16^{\prime}-6^{\prime \prime}$ | 15'-11" | 14'-11" |
|  | 360 | 17'-8' | $16^{\prime}-8^{\prime \prime}$ | $16^{\prime}-1{ }^{\prime \prime}$ | $15^{\prime}-5^{\prime \prime}$ | 18'-8' | 17'-5' | 16'-10" | 15'-10' | 17'-4'' | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-8" | 15'-1" | 18'-2' | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-5^{\prime \prime}$ | 15'-9'1 |
|  | 560 | 19'-3'' | 17'-10" | 17'-2' | $16^{\prime}-5^{\prime \prime}$ | 20'-5' | 18'-11' | $18^{\prime}-0^{\prime \prime}$ | 17'-2' | 18'-10' | $17^{\prime}-6^{\prime \prime}$ | $16^{\prime}-10^{\prime \prime}$ | $16^{\prime}-2{ }^{\prime \prime}$ | 19'-11' | 18'-5' | $17^{\prime}-8^{\prime \prime}$ | 16'-11' |
| 111/8" | 110 | 18'-8'' | $17^{\prime}-6^{\prime \prime}$ | $16^{\prime}-3^{\prime \prime}(1)$ | 14'-6"(1) | 19'-9' | 17'-10' | $16^{\prime}-3^{\prime \prime}(1)$ | $14^{\prime}-6^{\prime \prime}(1)$ | 18'-0' | $16^{\prime}-11^{\prime \prime}$ | $16^{\prime}-3^{\prime \prime}(1)$ | $14^{\prime}-6^{\prime \prime}(1)$ | 19'-0' | $17^{\prime}-8^{\prime \prime}$ | $16^{\prime}-3^{\prime \prime}(1)$ | 14'-6"(1) |
|  | 210 | 19'-3' | 17'-11" | $17^{\prime}-3^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ | 20'-4' | 18'-11' | 17'-10'(1) | $15^{\prime}-10^{\prime \prime}(1)$ | 18'-8' | $17^{\prime}-5^{\prime \prime}$ | $16^{\prime}-9{ }^{\prime \prime}$ | $15^{\prime}-10^{\prime \prime}(1)$ | 19'-8' | 18'-3'' | $17^{\prime}-6^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ |
|  | 230 | 19'-7' | 18'-3' | 17'-6" | 16'-9'(1) | 20'-9' | 19'-3" | 18'-5' | 16'-10'(1) | 19'-0" | $17^{\prime}-8^{\prime \prime}$ | $17^{\prime}-0^{\prime \prime}$ | $16^{\prime}-4^{\prime \prime}(1)$ | 20'-1' | 18'-7' | 17'-9" | $16^{\prime}-10^{\prime \prime}(1)$ |
|  | 360 | 20'-4' | 18'-11' | 18'-0' | 17'-3"'(1) | 21'-6' | 20'-0' | 19'-1' | $17^{\prime}-11^{\prime \prime}(1)$ | 19'-9" | 18'-4' | $17^{\prime}-7{ }^{\prime \prime}$ | $16^{\prime}-10^{\prime \prime}(1)$ | 20'-11' | 19'-4'' | $18^{\prime}-5^{\prime \prime}$ | 17'-7'(1) |
|  | 560 | 22'-3" | 20'-7' | 19'-7" | 18'-7' | 23'-7" | 21'-10'1 | 20'-9' | 19'-8' ${ }^{\prime \prime}$ (1) | 21'-9" | 20'-1' | 19'-2' | 18'-1' | 23'-0' | 21'-3' | 20'-3' | 19'-2" |
| 14" | 110 | 20'-9" | 19'-4'11) | 17'-9"(1) | 14'-6"(1) | 21'-11" | 19'-5"(1) | 17'-9'(1) | $14^{\prime}-6^{\prime \prime \prime}(1)$ | 20'-0' | 18'-7' | 17'-9'(1) | $14^{\prime}-6^{\prime \prime}(1)$ | 21'-1' | 19'-5'(1) | 17'-9'(1) | 14'-6"(1) |
|  | 210 | 21'-5' | 19'-11" | 19'-0'(1) | $15^{\prime}-10^{\prime \prime}$ | 22'-8' | 21-1'1(1) | $19^{\prime}-5^{\prime \prime}(1)$ | 15'-10'(1) | 20'-8' | 19'-2' | $18^{\prime}-3^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ | 21'-10" | 20'-3" | $19^{\prime}-4^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ |
|  | 230 | 21'-10" | 20'-3' | $19^{\prime}-4^{\prime \prime}(1)$ | $17^{\prime}-0^{\prime \prime}(1)$ | $23^{\prime}-1{ }^{\prime \prime}$ | 21'-5" | $20^{\prime}-6^{\prime \prime}(1)$ | 17'-7'(1) | 21'-1" | 19'-7' | $18^{\prime}-8^{\prime \prime}$ | $17^{\prime}-0^{\prime \prime}(1)$ | 22'-4' | 20'-8' | $19^{\prime}-8^{\prime \prime}(1)$ | 17'-7'(1) |
|  | 360 | 22'-7' | 21'-0' | 20'-0'(1) | 17-4'1(1) | 23'-11" | 22'-2' | 21'-2'11 | $17^{\prime}-11^{\prime \prime}(1)$ | 22'-0" | 20'-4' | 19'-4' | $17^{\prime}-4^{\prime \prime}(1)$ | $23^{\prime}-2{ }^{\prime \prime}$ | 21'-6" | 20'-6'(1) | 17'-11"(1) |
|  | 560 | 24'-9"' | 22'-11" | 21'-9" | $20^{\prime}-4^{\prime \prime}(1)$ | 26'-2' | 24'-3" | 23'-1' | 21-10'1(1) | $24^{\prime}-2{ }^{\prime \prime}$ | 22'-4" | 21'-3' | 20'-1 ${ }^{\prime \prime}$ (1) | 25'-7" | 23'-7' | 22'-5' | 21'-2"(1) |
| 16" | 210 | 23'-4" | 21'-8'1(1) | 19'-11'(1) | 15'-10'1(1) | 24'-8" | 22'-10'(1) | 19'-11'(1) | 15'-10'1(1) | 22'-6" | 20'-10'(1) | 19'-11'(1) | 15'-10'(1) | 23'-9" | 22'-1'11) | 19'-11'(1) | 15'-10'1(1) |
|  | 230 | 23'-9'' | 22'-1' | 21-1'1) | $17^{\prime}-0^{\prime \prime}(1)$ | $25^{\prime}-1{ }^{\prime \prime}$ | $23^{\prime}-4^{\prime \prime}(1)$ | 21'-11"(1) | 17'-7'(1) | 23'-0" | 21'-3' | 20'-3'11) | $17^{\prime}-0^{\prime \prime}(1)$ | 24'-3' | 22'-6" | 21'-5'(1) | 17'-7'(1) |
|  | 360 | 24'-7' | 22'-10'1 | 21'-9"(1) | 17-4'1(1) | $26^{\prime}-0^{\prime \prime}$ | 24'-2" ${ }^{\text {(1) }}$ | $22^{\prime}-5^{\prime \prime}(1)$ | $17^{\prime}-11^{\prime \prime}(1)$ | 23'-11" | $22^{\prime}-1{ }^{\prime \prime}$ | 21'-1'11) | $17^{\prime}-4^{\prime \prime}(1)$ | $25^{\prime}-3^{\prime \prime}$ | $23^{\prime}-4{ }^{\prime \prime}$ | $22^{\prime}-3^{\prime \prime}(1)$ | $17^{\prime}-11^{1 \prime(1)}$ |
|  | 560 | 26'-11' | 24'-11' | 23'-9" | $20^{\prime}-4^{\prime \prime}(1)$ | 28'-6' | $26^{\prime}-4{ }^{\prime \prime}$ | $25^{-1}-1^{1(1)}$ | $22^{\prime}-1^{\prime \prime}(1)$ | $26^{\prime}-4^{\prime \prime}$ | $24^{\prime}-3^{\prime \prime}$ | 23'-1' | $20^{\prime}-4^{\prime \prime}(1)$ | 27'-10' | $25^{\prime}-8{ }^{\prime \prime}$ | $24^{\prime}-5^{\prime \prime}(1)$ | $22^{\prime}-1^{\prime \prime}(1)$ |

(1) Web stiffeners are required at intermediate supports of continuous-span joists when the intermediate bearing length is less than $51 / 4 / 4$ and the span on either side of the intermediate bearing is greater than the following spans:

| 40 PSF Live Load / 15 PSF Dead Load |  |  |  |  | 40 PSF Live Load / 30 PSF Dead Load |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TJI® | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 110 | Not Required |  | 19'-3' | 15'-4' | Not Required | 18'-8" | 15'-6" | 12'-5" |
| 210 |  |  | 21'-4" | 17'-1' |  | 20'-8" | 17'-3" | $13^{\prime \prime}$-9' |
| 230 |  |  |  | 19'-2' |  | 23'-3" | 19'-4" | 15'-5" |
| 360 |  |  |  | 19'-7" |  | 23'-9" | 19'-9" | 15'-10" |
| 560 |  |  |  |  |  |  | 24'-2" | 19'-3" |

> To more accurately predict floor performance, use our TJ-Pro ${ }^{T M}$ Ratings

- Bold italic spans indicate floors that would meet National Building Code of Canada (NBCC) vibration criteria but would be considered by 35\% of the population to have marginal or unacceptable performance


## General Notes

- Tables are based on:
- Clear distance between supports.
- Minimum bearing length of $13 / 4$ " end (no web stiffeners) and $31 / 2^{\prime \prime}$ intermediate.
- Limit States Design per CSA 086.
- Uniform loads.
- Single layer of appropriate span-rated OSB.
- NBCC vibration criteria as ratified by Canadian Construction Materials Centre (CCMC).
- Long term deflection under dead load, which includes the effect of creep, has not been considered.
- For continuous spans, ratio of short span to long span should be 0.4 or greater to prevent uplift.
- Spans generated from Weyerhaeuser software may exceed the spans shown in these tables because software reflects actual design conditions.
- For multi-family applications and other loading conditions not shown, refer to Weyerhaeuser software.


## See page 7 for how to use these tables.

7/8" OSB Subfloor (Glue-nailed)—Vibration-Controlled, Standard Term

| Depth | TJ® | Directly Applied Ceiling |  |  |  |  |  |  |  | No Directly Applied Ceiling |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Simple or Continuous Span |  |  |  | Continuous Span Only |  |  |  | Simple or Continuous Span |  |  |  | Continuous Span Only |  |  |  |
|  |  | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 40 PSF Live Load / 15 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91/2" | 110 | 17'-3' | 15'-10'1 | 14'-10' | $13^{\prime}-8^{\prime \prime}$ | $18^{\prime}-0{ }^{\prime \prime}$ | 17'-1" | $16^{\prime}-1{ }^{1 \prime}$ | 14'-5' | 16'-9' | 15'-10' | 14'-10" | $13^{\prime \prime}-8^{\prime \prime}$ | $17^{\prime}-6^{\prime \prime}$ | 16'-6' | 15'-11' | 14'-5' |
|  | 210 | 17'-8' | 16'-8' | 15'-8' | 14'-5' | 18'-7' | 17'-6' | 16'-10' | 15'-9' | 17'-3' | 16'-3' | 15'-8' | 14'-5' | 18'-0' | 17'-0' | $16^{\prime}-4{ }^{\prime \prime}$ | 15'-8" |
|  | 230 | 17'-11" | $16^{\prime}-11^{\prime \prime}$ | $16^{\prime}-2{ }^{\prime \prime}$ | 14'-11" | 19'-0' | 17'-9" | 17'-1' | $16^{\prime}-4{ }^{\prime \prime}$ | $17^{\prime}-6^{\prime \prime}$ | $16^{\prime}-7{ }^{\prime \prime}$ | $15^{\prime}-11^{\prime \prime}$ | 14'-11" | 18'-5' | $17^{\prime}-3^{\prime \prime}$ | $16^{\prime}-8{ }^{\prime \prime}$ | 15'-11' |
|  | 360 | 18'-7' | 17'-5' | $16^{\prime}-9$ ' | 15'-11' | 19'-8' | 18'-4' | $17^{\prime}-6^{\prime \prime}$ | 16'-9' | 18'-2' | $17^{\prime}-1{ }^{\prime \prime}$ | $16^{\prime}-5^{\prime \prime}$ | $15^{\prime}-8^{\prime \prime}$ | 19'-2' | 17'-10' | $17^{\prime}-2^{\prime \prime}$ | 16'-4' |
|  | 560 | 20'-4' | 18'-10" | 17'-11' | 17'-1' | $21^{\prime}-6^{\prime \prime}$ | 19'-11' | 19'-0' | 17'-11' | 19'-11" | 18'-5' | 17'-7' | $16^{\prime}-10^{\prime \prime}$ | 21'-0' | 19'-6' ${ }^{\prime \prime}$ | $18^{\prime}-6^{\prime \prime}$ | 17'-7'1 |
| 117/8" | 110 | 19'-8' | 18'-4' | 17'-7' | $16^{\prime}-2^{\prime \prime}(1)$ | 20'-10" | 19'-5' | 18'-1' | $16^{\prime}-2^{\prime \prime}(1)$ | 19'-0' | 17'-9' | 17'-1' | $16^{\prime}-2^{\prime \prime}(1)$ | 20'-1' | 18'-8' | 17'-10" | 16'-2'(1) |
|  | 210 | 20'-4' | 18'-11" | 18'-1' | 17'-3'11) | 21'-6" | $20^{\prime}-0^{\prime \prime}$ | 19'-1' | 17'-9'(1) | 19'-8' | 18'-3' | 17'-6' | $16^{\prime}-9{ }^{\prime \prime}$ | 20'-9' | $19^{\prime}-4^{\prime \prime}$ | 18'-5' | $17^{\prime}-6^{\prime \prime \prime}(1)$ |
|  | 230 | 20'-8' | 19'-3' | $18^{\prime}-4^{\prime \prime}$ | 17'-6' | 21'-10' | 20'-4' | 19'-5' | 18'-4' | 20'-1' | $18^{\prime}-8^{\prime \prime}$ | 17'-9' | 17'-0'' | 21'-2' | 19'-8' | $18^{\prime}-9{ }^{\prime \prime}$ | 17'-9'' |
|  | 360 | $21^{\prime \prime} 5^{\prime \prime}$ | 19'-11" | 19'-0' | 17'-11" | 22'-8' | 21'-1' | 20'-1' | 19'-0' | 20'-11" | 19'-4' | 18'-5' | 17'-6" | 22'-1' | 20'-6" | 19'-6' | 18'-4' |
|  | 560 | $23^{\prime}-5^{\prime \prime}$ | 21'-9" | 20'-8' | 19'-6" | 24'-9" | $23^{\prime}-0^{\prime \prime}$ | 21'-11' | 20'-7' | 22'-11' | $21^{\prime}-3^{\prime \prime}$ | 20'-2' | $19^{\prime}-0^{\prime \prime}$ | 24'-3' | 22'-5' | 21'-4' | $20^{\prime}-1{ }^{\prime \prime}$ |
| 14" | 110 | 21'-11" | 20'-5' | 19'-6'(1) | 17'-8'(1) | 23'-1' | 21'-7' | 19'-9'(1) | 17'-8'(1) | 21'-1' | 19'-7" | 18'-8' | 17'-8'1(1) | 22'-3' | 20'-8' | 19'-9'(1) | 17'-8'(1) |
|  | 210 | 22'-7' | $21^{\prime}-0^{\prime \prime}$ | 20'-1' | 18'-11'(1) | 23'-10" | 22'-3' | 21'-3' | $19^{\prime}-4^{\prime \prime}(1)$ | 21'-10" | 20'-3' | 19'-4' | 18'-3 ${ }^{\prime \prime}$ (1) | 23'-1' | 21'-5' | 20'-5' | $19^{\prime}-3^{\prime \prime \prime}(1)$ |
|  | 230 | $23^{\prime}-0^{\prime \prime}$ | 21'-5' | 20'-5' | 19'-3'11) | $24^{\prime}-3^{\prime \prime}$ | 22'-8' | 21'-7' | 20'-5'(1) | 22'-3' | $20^{\prime}-8^{\prime \prime}$ | 19'-8' | 18'-7' | 23'-6" | 21'-10" | 20'-10' | 19'-7'(1) |
|  | 360 | 23'-10' | 22'-2' | 21'-1' | 19'-11'(1) | 25'-2' | 23'-5' | 22'-4' | 21'-1'(1) | 23'-2' | 21'-6' | 20'-5' | 19'-3' | 24'-6" | 22'-8' | 21'-7' | 20'-4"(1) |
|  | 560 | 26'-0' | 24'-2' | 22'-11' | 21'-7" | $27^{\prime}-6^{\prime \prime}$ | 25'-6" | 24'-3' | 22'-10" | 25'-6" | 23'-7" | 22'-5' | 21'-1' | 26'-11' | 24'-11" | 23'-8' | 22'-3'1 |
| $16 "$ | 210 | 24'-7' | 22'-11" | 21'-10'(1) | 19'-8'(1) | 25'-11" | 24'-2' | 23'-1'11) | 19'-8'(1) | 23'-9" | 22'-1' | 21'-0' | 19'-8'1(1) | 25'-1' | 23'-3" | 22'-2'(1) | $19^{\prime}-8^{\prime \prime}(1)$ |
|  | 230 | $25^{\prime}-0^{\prime \prime}$ | $23^{\prime}-4^{\prime \prime}$ | 22'-3' | $21^{\prime}-0^{\prime \prime}(1)$ | $26^{\prime}-5^{\prime \prime}$ | 24'-8' | $23^{\prime}-6^{\prime \prime}$ | 21-10'11) | 24'-3' | 22'-6" | 21'-5' | 20'-2'11) | 25'-7' | 23'-9" | $22^{\prime}-7{ }^{\prime \prime}$ | 21-4'1(1) |
|  | 360 | 25'-11" | 24'-1' | 23'-0' | $21^{\prime}-6^{\prime \prime}(1)$ | $27^{\prime}-4^{\prime \prime}$ | 25'-6" | $24^{\prime}-4{ }^{\prime \prime}$ | $22^{\prime}-2^{\prime \prime}(1)$ | $25^{\prime}-2^{\prime \prime}$ | $23^{\prime}-4^{\prime \prime}$ | 22'-3' | 20'-11'(1) | 26'-7' | 24'-8' | $23^{\prime}-6^{\prime \prime}$ | 22'-1'(1) |
|  | 560 | 28'-3' | $26^{\prime}-3$ ' | 25'-0' | 23'-6' | 29'-11" | 27'-9" | 26'-5' | 24'-11'(1) | 27'-8' | 25'-7' | 24'-4' | 22'-11' | 29'-3' | 27'-1' | 25'-9' | 24'-2'(1) |
| 40 PSF Live Load / 30 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 91/2" | 110 | 17'-3' | 15'-10" | $14^{\prime}-6^{\prime \prime}$ | 12'-5' | 18'-0' | 15'-10" | $14^{\prime}-6^{\prime \prime}$ | 12'-5' | 16'-9' | 15'-10'\| | 14-6 | $12-5$ | 17-6 | 15'-10" | $14^{\prime}-6^{\prime \prime}$ | 12'-5' |
|  | 210 | 17'-8' | $16^{\prime}-8^{\prime \prime}$ | $15^{\prime}-8{ }^{\prime \prime}$ | 13'-9' | 18'-7" | 17'-5' | 15'-10' | 13'-9' | 17'-3' | $16^{\prime}-3^{\prime \prime}$ | 15'-8' | 13'-9' | 18'-0' | $17^{\prime}-0^{\prime \prime}$ | 15'-10' | 13'-9'' |
|  | 230 | 17'-11" | $16^{\prime}-11^{\prime \prime}$ | $16^{\prime}-2^{\prime \prime}$ | $14^{\prime}-11^{\prime \prime}$ | 19'-0' | 17'-9' | $16^{\prime}-9^{\prime \prime}$ | 14'-11" | $17^{\prime}-6^{\prime \prime}$ | $16^{1}-7^{\prime \prime}$ | $15^{\prime}-11^{\prime \prime}$ | 14'-11" | 18'-5' | $17^{1}-3{ }^{\prime \prime}$ | $16^{\prime}-8{ }^{\prime \prime}$ | 14'-11" |
|  | 360 | 18'-7' | $17^{\prime}-5^{\prime \prime}$ | $16^{\prime}-9$ ' | 15'-10'1 | 19'-8' | 18'-4' | $17^{\prime}-6^{\prime \prime}$ | 15'-10' | 18'-2' | $17^{\prime}-1{ }^{\prime \prime}$ | $16^{\prime}-5^{\prime \prime}$ | $15^{\prime}-8^{\prime \prime}$ | 19'-2' | 17'-10" | $17^{\prime}-2^{\prime \prime}$ | 15'-10" |
|  | 560 | 20'-4' | 18'-10" | 17'-11' | 17'-1' | 21'-6" | 19'-11" | $19^{\prime}-0^{\prime \prime}$ | 17'-11' | 19'-11" | 18'-5' | 17'-7' | $16^{\prime}-10^{\prime \prime}$ | 21'-0' | 19'-6" | $18^{\prime}-6^{\prime \prime}$ | 17'-7' |
| 117/8" | 110 | 19'-8' | 17'-10' | $16^{\prime}-3^{\prime \prime}(1)$ | 14'-6 ${ }^{\prime \prime}$ (1) | 20'-7' | 17'-10' | 16'-3'11) | $14^{\prime}-6^{\prime \prime}(1)$ | 19'-0" | 17'-9' | $16^{\prime}-3^{\prime \prime}(1)$ | $14^{\prime}-6^{\prime \prime}(1)$ | 20'-1' | 17'-10" | $16^{\prime}-3^{\prime \prime}(1)$ | $14^{\prime}-6^{\prime \prime}(1)$ |
|  | 210 | $20^{\prime}-4{ }^{\prime \prime}$ | 18'-11' | 17'-10'(1) | $15^{\prime}-10^{\prime \prime}(1)$ | $21^{\prime}-6^{\prime \prime}$ | 19'-7" | $17^{\prime}-10^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ | 19'-8' | $18^{\prime}-3^{\prime \prime}$ | $17^{\prime}-6^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ | 20'-9' | 19'-4' | 17'-10'(1) | $15^{\prime}-10^{\prime \prime}(1)$ |
|  | 230 | $20^{\prime}-8^{\prime \prime}$ | 19'-3' | 18'-4' | $16^{\prime}-10^{\prime \prime}(1)$ | 21'-10" | 20'-4' | 18'-10' | $16^{\prime}-10^{\prime \prime}(1)$ | $20^{\prime}-1{ }^{\prime \prime}$ | $18^{\prime}-8^{\prime \prime}$ | $17^{\prime}-9$ ' | $16^{\prime}-10^{\prime \prime}(1)$ | $21^{\prime}-2$ ' | 19'-8' | 18'-9' | $16^{\prime}-10^{1 \prime(1)}$ |
|  | 360 | 21'-5' | 19'-11' | 19'-0' | $17^{\prime}-4^{\prime \prime}(1)$ | 22'-8' | 21-1' | $20^{\prime}-1^{\prime \prime}(1)$ | $17^{\prime}-11^{\prime \prime}(1)$ | 20'-11' | 19'-4' | $18^{\prime}-5^{\prime \prime}$ | 17'-4'1) | 22'-1' | 20'-6' | $19^{\prime}-6^{\prime \prime}$ | 17'-11'(1) |
|  | 560 | $23^{\prime}-5^{\prime \prime}$ | 21'-9" | 20'-8' | 19'-6'(1) | 24'-9" | $23^{\prime}-0^{\prime \prime}$ | 21'-11' | 20'-7' ${ }^{(1)}$ | 22'-11" | $21^{\prime}-3^{\prime \prime}$ | $20^{\prime}-2^{\prime \prime}$ | 19'-0' | $24^{\prime}-3^{\prime \prime}$ | $22^{\prime}-5^{\prime \prime}$ | $21^{\prime}-4{ }^{\prime \prime}$ | 20'-1'(1) |
| 14" | 110 | 21'-11" | 19'-5"(1) | 17'-9'(1) | 14'-6 ${ }^{\prime \prime}$ (1) | 22'-5' | 19'-5"(1) | 17'-9'1(1) | $14^{\prime}-6^{\prime \prime}(1)$ | 21'-1' | 19'-5'1(1) | 17'-9'(1) | $14^{\prime}-6^{\prime \prime}(1)$ | 22'-3' | 19'-5"(1) | 17'-9'(1) | 14'-6 ${ }^{1 \prime(1)}$ |
|  | 210 | 22'-7' | 21'-0"(1) | $19^{\prime}-5^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ | 23'-10" | 21-4'(1) | 19'-5'(1) | $15^{\prime}-10^{\prime \prime}(1)$ | 21'-10' | 20'-3' | $19^{\prime}-4^{\prime \prime}(1)$ | $15^{\prime}-10^{\prime \prime}(1)$ | 23'-1' | 21'-4'(1) | $19^{\prime}-5^{\prime \prime}(1)$ | $15^{1}-10^{1 /(1)}$ |
|  | 230 | $23^{\prime}-0^{\prime \prime}$ | 21'-5' | $20^{\prime}-5^{\prime \prime}(1)$ | $17^{\prime}-0^{\prime \prime}(1)$ | $24^{\prime}-3^{\prime \prime}$ | $22^{\prime}-5^{\prime \prime}$ | 20'-6 $6^{\prime \prime}$ (1) | 17'-7'1(1) | $22^{\prime}-3^{\prime \prime}$ | $20^{\prime}-8^{\prime \prime}$ | $19^{\prime}-8^{\prime \prime}(1)$ | $17^{\prime}-0^{\prime \prime}(1)$ | $23^{\prime}-6^{\prime \prime}$ | 21'-10" | 20'-6'11) | 17'-7'(1) |
|  | 360 | 23'-10'1 | $22^{\prime}-2{ }^{\prime \prime}$ | 21-1'1(1) | $17^{\prime}-4^{\prime \prime}(1)$ | $25^{\prime}-2^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | $22^{\prime}-4^{\prime \prime}(1)$ | $17^{\prime}-11^{\prime \prime}(1)$ | $23^{\prime}-2^{\prime \prime}$ | $21^{\prime}-6^{\prime \prime}$ | 20'-5'11) | $17^{\prime}-4^{\prime \prime}(1)$ | $24^{\prime}-6{ }^{\prime \prime}$ | 22'-8' | 21'-7'(1) | $17^{\prime}-11^{1 \prime(1)}$ |
|  | 560 | 26'-0' | 24'-2' | 22'-11" | 20'-4'(1) | 27'-6" | 25'-6" | 24'-3'(1) | 22'-1 $1^{\prime \prime}(1)$ | $25^{\prime}-6^{\prime \prime}$ | 23'-7" | 22'-5" | $20^{\prime}-4^{\prime \prime}(1)$ | 26'-11' | 24'-11" | $23^{\prime}-8^{\prime \prime}$ | 22'-1 ${ }^{\prime \prime}$ (1) |
| $16^{\prime \prime}$ | 210 | $24^{\prime}-7{ }^{\prime \prime}$ | 22'-10'(1) | 19'-11'(1) | $15^{1}-10^{\prime \prime}(1)$ | 25'-11" | 22'-10 ${ }^{1 \prime}$ (1) | 19'-11'(1) | $15^{\prime}-10^{\prime \prime}(1)$ | 23'-9" | 22'-1'1(1) | 19'-11"(1) | $15^{\prime}-10^{\prime \prime}(1)$ | $25^{\prime}-1{ }^{\prime \prime}$ | $22^{\prime}-10^{\prime \prime}(1)$ | 19'-11'(1) | $15^{1}-10^{11(1)}$ |
|  | 230 | 25'-0' | $23^{\prime}-4^{\prime \prime}(1)$ | 21'-4'(1) | $17^{\prime}-0^{\prime \prime}(1)$ | $26^{\prime}-5^{\prime \prime}$ | $24^{\prime}-0^{\prime \prime}(1)$ | 21-11'(1) | 17'-7'(1) | 24'-3" | 22'-6' | $21^{\prime}-4^{\prime \prime}(1)$ | $17^{\prime}-0^{\prime \prime}(1)$ | 25'-7' | 23'-9'(1) | 21-11"(1) | 17'-7'(1) |
|  | 360 | $25^{\prime}-11^{\prime \prime}$ | $24^{\prime}-1^{\prime \prime}(1)$ | $21^{\prime}-9^{\prime \prime}(1)$ | $17^{\prime}-4^{\prime \prime}(1)$ | $27^{\prime}-4{ }^{\prime \prime}$ | $25^{\prime}-6^{\prime \prime}(1)$ | $22^{1}-5^{\prime \prime}(1)$ | 17'-11'(1) | $25^{\prime}-2^{\prime \prime}$ | $23^{\prime}-4{ }^{\prime \prime}$ | 21'-9'(1) | $17^{\prime}-4^{\prime \prime}(1)$ | $26^{\prime}-7{ }^{\prime \prime}$ | $24^{\prime}-8^{\prime \prime}(1)$ | $22^{\prime}-5^{\prime \prime}(1)$ | $17^{\prime}-11^{1 \prime(1)}$ |
|  | 560 | 28'-3" | $26^{\prime}-3^{\prime \prime}$ | $25^{\prime}-0^{\prime \prime}(1)$ | 20'-4'(1) | 29'-11" | 27'-9' | $26^{\prime}-5^{\prime \prime}(1)$ | 22'-1"(1) | $27^{\prime}-8^{\prime \prime}$ | $25^{\prime}-7{ }^{\prime \prime}$ | 24'-4'(1) | $20^{\prime}-4^{\prime \prime}(1)$ | 29'-3' | 27'-1' | 25'-9'(1) | $22^{\prime}-1^{\prime \prime}(1)$ |

(1) Web stiffeners are required at intermediate supports of continuous-span joists when the intermediate bearing length is less than $51 / 4$ " and the span on either side of the intermediate bearing is greater than the following spans:

| 40 PSF Live Load / 15 PSF Dead Load |  |  |  |  | 40 PSF Live Load / 30 PSF Dead Load |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TJI® | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 12" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 110 | Not Required |  | 19'-3' | 15'-4" | Not Required | 18'-8" | 15'-6" | 12'-5" |
| 210 |  |  | 21'-4" | 17'-1' |  | 20'-8" | 17'-3" | 13'-9" |
| 230 |  |  |  | 19'-2' |  | 23'-3" | 19'-4" | 15'-5" |
| 360 |  |  |  | 19'-7" |  | 23'-9" | 19'-9" | 15'-10" |
| 560 |  |  |  | 23'-11' |  |  | 24'-2" | 19'-3" |

> To more accurately predict floor performance, use our TJ-Pro ${ }^{T M}$ Ratings

- Bold italic spans indicate floors that would meet National Building Code of Canada (NBCC) vibration criteria but would be considered by 35\% of the population to have marginal or unacceptable performance.


## See pages 7 and 8 for how to use these tables and General Notes.

## These Conditions Are NOT Permitted:



DO NOT use sawn lumber for rim board or blocking as it may shrink after installation. Use only engineered lumber


DO NOT bevel cut
joist beyond inside face of wall.


DO NOT install hanger overhanging face of plate or beam. Flush bearing plate with inside face of wall or beam.

Cantilevers Less than 5" (Brick Ledge) See Section A of cantilever table on page 11
 when supporting roof load, assuming:

- simple or continuous span
- $\mathrm{L}_{1} \leq \mathrm{L}_{2}$
- minimum backspan $=2 x$ cantilever length

Cantilevers 5" to 24"
See Section B of cantilever table on page 11


TJI® joists may be cantilevered 5 " to 24 "
when supporting roof load, assuming:

- simple or continuous span
- $\mathrm{L}_{1} \leq \mathrm{L}_{2}$
- minimum backspan $=2 x$ cantilever length

PB1
Cantilever back span must be permanently braced with either direct-applied ceiling along entire length or permanent bracing at $1 / 3$ points. See detail PB1 below for connections.

E1, E1W
Web stiffeners required both sides at E1W

ONLY
$8^{\text {" }}$ diameter maximum hole for $117 / 8^{\prime \prime}-16^{\text {" deep blocking }}$ panels; 6 " diameter maximum for blocking panels $91 / 2{ }^{\prime \prime}$ deep or shorter than $12^{\prime \prime}$ long. Do not cut flanges.

11/8" TJ® Rim Board, 11/4" or $11 / 2^{\prime \prime}$ TimberStrand ${ }^{\circledR}$ LSL, typical. Nail with ( $0.131^{\prime \prime} \times 3$ ") nails, one each at top and bottom flange.

E5, E6
Full depth vertical blocking panel between each joist. Use 12 " length of $3 / 4$ " reinforcement on one side at E5, both sides at E6. Attach to joist with one $8 \mathrm{~d}\left(0.131^{\prime \prime} \times 2 \frac{1}{2} 2^{\prime \prime}\right)$ nail at each corner.

Details E2-E9 are not for use with joist depths > 16".
See pages 20-21 for cantilevers using deeper joists.
For more information on details E1-EG, refer to our cover sheets and AutoCAD details online at weyerhaeuser.com/woodproducts/software-learning.


Directly applied ceiling
When specified on the layout, one of the above bracing options is required

## Cantilever Reinforcement

| Depth | TJ® | $\begin{aligned} & \text { Roof } \\ & \text { Truss } \\ & \text { Span } \end{aligned}$ | Section A: Cantilevers less than 5" (Brick Ledge) |  |  |  |  |  |  |  |  | Section B: Cantilevers 5" to 24" |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Unfactored Roof Total Load |  |  |  |  |  |  |  |  | Unfactored Roof Total Load |  |  |  |  |  |  |  |  |
|  |  |  | 35 PSF |  |  | 45 PSF |  |  | 55 PSF |  |  | 35 PSF |  |  | 45 PSF |  |  | 55 PSF |  |  |
|  |  |  | On-Centre Joist Spacing |  |  |  |  |  |  |  |  | On-Centre Joist Spacing |  |  |  |  |  |  |  |  |
|  |  |  | 16" | 19.2" | 24" | $16{ }^{\prime \prime}$ | 19.2" | $24 "$ | $16{ }^{\prime \prime}$ | 19.2" | 24" | $16{ }^{\prime \prime}$ | 19.2" | $24 "$ | 16 " | 19.2" | $24{ }^{\prime \prime}$ | $16 "$ | 19.2" | 24" |
| $\begin{gathered} 91 / 2 " \\ 111 / \mathbf{n}^{\prime \prime} \\ 14^{\prime \prime} \end{gathered}$ | 110 | 18' |  |  |  |  |  | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | X |
|  |  | $20^{\prime}$ |  |  | E5 |  | E5 | E5 |  | E5 | E5 |  |  |  |  |  | E2 |  | E2 | X |
|  |  | $22^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  |  |  |  | X |  | E3 | X |
|  |  | $24^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  | E2 |  | E2 | X | E2 | X | X |
|  |  | $26^{\prime}$ |  | E5 | E5 | E5 | E5 | E5 | E5 | E5 | E6 |  |  | E3 | E2 | E3 | X | E3 | X | X |
|  |  | $28^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  | E2 | X | E2 | X | X | X | X | X |
|  |  | $30^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  | E3 | X | E3 | X | X | X | X | X |
| $\begin{gathered} 91 / 2 " \\ 11 /{ }^{\prime \prime \prime} \\ 1444^{\prime \prime} \\ 16 " \end{gathered}$ | 210 | $18^{\prime}$ |  |  |  |  |  | E5 |  |  | E5 |  |  |  |  |  |  |  |  | E2 |
|  |  | $20^{\prime}$ |  |  |  |  |  | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E2 |
|  |  | 22' |  |  | E5 |  | E5 | E5 |  | E5 | E5 |  |  |  |  |  | E2 |  | E2 | E3 |
|  |  | $24^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  |  |  |  | E3 |  | E3 | X |
|  |  | $26^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  | E2 |  | E2 | x | E2 | E3 | X |
|  |  | $28^{\prime}$ |  | E5 | E5 | E5 | E5 | E5 | E5 | E5 | E6 |  |  | E3 |  | E3 | X | E3 |  | X |
|  |  | $30^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  | E2 | E3 | E2 | X | X | X | X | X |
|  |  | 32' |  | X | X | E5 | X | X | E5 | X | X |  | E2 | X | E3 | X | X | X | X | X |
| $\begin{gathered} 91 /{ }^{\prime \prime \prime} \\ 111^{\prime \prime} \\ 14^{\prime \prime} \\ 16^{\prime \prime} \end{gathered}$ | 230 | $20^{\prime}$ |  |  |  |  |  | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E2 |
|  |  | 22' |  |  | E5 |  | E5 | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E3 |
|  |  | $24^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  |  |  |  | E2 |  | E2 | X |
|  |  | $26^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  |  |  |  | E3 | E2 | E3 | X |
|  |  | 28 |  | E5 | E5 | E5 | E5 | E5 | E5 | E5 | E5 |  |  | E2 |  | E2 | X | E2 | X | X |
|  |  | $30^{\prime}$ |  | E5 | E5 | E5 | E5 | E5 | E5 | E5 | E6 |  |  | E3 | E2 | E3 | X | E3 | X | X |
|  |  | $32^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  | E2 | X | E2 | X | X | X | X | X |
| $\begin{gathered} 91 / 2 " 1 \\ 111 /{ }^{\prime \prime \prime} \\ 144 \\ 16 " \end{gathered}$ | 360 | $22^{\prime}$ |  |  |  |  |  | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E2 |
|  |  | $24^{\prime}$ |  |  | E5 |  | E5 | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E3 |
|  |  | $26^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  |  |  |  | E2 |  | E2 | X |
|  |  | $28^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E5 |  |  |  |  |  | E3 |  | E3 | X |
|  |  | $30^{\prime}$ |  | E5 | E5 |  | E5 | E5 | E5 | E5 | E6 |  |  | E2 |  | E2 | X | E2 | X | X |
|  |  | 32' |  | E5 | E5 | E5 | E5 | E5 | E5 | E5 | E6 |  |  | E3 |  | E3 | x | E3 | X | X |
|  |  | $34^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  | E2 | X | E2 | E3 | X | X | X | X |
|  |  | $36^{\prime}$ |  | X | X | E5 | X | X | E5 | X | X |  | E2 | X | E3 | X | X | X | X | X |
| $\begin{gathered} 91 /{ }^{\prime \prime \prime} \\ 11 /{ }^{\prime \prime \prime} \\ 14^{\prime \prime} \\ 16 " \end{gathered}$ | 560 | $26^{\prime}$ |  |  |  |  |  | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E2 |
|  |  | $28^{\prime}$ |  |  | E5 |  |  | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E2 |
|  |  | $30^{\prime}$ |  |  | E5 |  | E5 | E5 |  | E5 | E5 |  |  |  |  |  |  |  |  | E3 |
|  |  | $32^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E6 |  |  |  |  |  | E2 |  | E2 | E3 |
|  |  | $34^{\prime}$ |  |  | E5 |  | E5 | E5 | E5 | E5 | E6 |  |  |  |  |  | E3 |  | E2 | X |
|  |  | $36^{\prime}$ |  | E5 | E5 |  | E5 | E5 | E5 | E5 | E6 |  |  |  |  | E2 | E3 | E2 | E3 | X |
|  |  | $38^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  |  | E2 |  | E2 | X | E2 | X | X |
|  |  | $40^{\prime}$ |  | E5 | X | E5 | E5 | X | E5 | E5 | X |  |  | X |  | E3 | X | E3 | X | X |

## How to Use This Table

1. Identify $T J \otimes^{®}$ joist and depth.
2. Locate the Roof Truss Span (horizontal) that meets or exceeds your condition.
3. Identify the cantilever condition (less than $5^{\prime \prime}$ or $5^{\prime \prime}$ to 24 ") and locate the Unfactored Roof Total Load and On-Centre Joist Spacing for your application.
4. Scan down to find the appropriate cantilever detail and refer to drawing on page 10:

- Blank cells indicate no reinforcement is required.
- E4 may be used in place of E2 or E3 except when using TJI® 560 joists.
- X indicates cantilever will not work. Use ForteWEBTM or Javelin ${ }^{\circledR}$ Software, or reduce spacing of joists and recheck table.


## General Notes

- Table is based on:
- 15 psf unfactored roof dead load on a horizontal projection.
- 80 plf unfactored exterior wall load with 3'-0" maximum width window or door openings. For larger openings, or multiple $3^{\prime}-0$ " width openings spaced less than $6^{\prime}-0$ " on-centre, additional joists beneath the opening's trimmers may be required.
- 40/15 psf floor load.
- More restrictive of simple or continuous span.
- Roof truss with 24" soffits.
- $3 / 4$ " reinforcement refers to $3 / 4$ " standard sheathing grade of Douglas fir or Canadian softwood plywood or other $3 / 4 / 4$ exterior grade 48/24-rated sheathing that is cut to match the full depth of the $\mathrm{TJ}{ }^{\circledR}$ joist. Install with face grain horizontal. Reinforcing member must bear fully on the wall plate.
- Designed for $2 \times 4$ and $2 \times 6$ plate widths.
- For conditions beyond the scope of this table, including cantilevers longer than 24 ", use our ForteWEBTM or Javelin ${ }^{\circledR}$ software.


## Roof-Maximum Horizontal Clear Spans, Standard Term

| $\begin{gathered} \text { O.C. } \\ \text { Spacing } \end{gathered}$ | Depth | TJ ${ }^{\text {® }}$ | Unfactored Snow Load (LL) and Dead Load (DL) in PSF |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 25LL + 15DL |  | 30LL + 15DL |  | 40LL + 15DL |  | 50LL + 15DL |  |
|  |  |  | Low | High | Low | High | Low | High | Low | High |
| 16" | 91⁄2" | 110 | 18'-0" | 16'-8" | 16'-11" | 15'-8" | 15'-3" | 14'-2" | 14'-1' | 13'-1" |
|  |  | 210 | 19'-0" | 17'-8" | 17'-10" | 16'-7" | 16'-2" | 15'-0" | 14'-11" | 13'-11" |
|  |  | 230 | 19'-8" | 18'-3" | 18'-6" | 17'-2" | 16'-8" | 15'-6" | 15'-5" | 14'-4" |
|  |  | 360 | 20'-11" | 19'-5" | 19'-8" | 18'-3" | 17'-9" | 16'-6" | 16'-5" | 15'-3" |
|  |  | 560 | 24'-1" | 22'-5" | 22'-7" | 21'-0" | 20'-5" | 19'-0" | 18'-11" | 17'-7" |
|  | 117/8" | 110 | 21'6" | 19'-11" | 20'-2" | 18'-9" | 18'-3" | 17'-0" | $16^{\prime}-11^{\prime \prime}$ | 15'-8" |
|  |  | 210 | 22'-9" | 21'-1" | 21-4" | 19'-10" | 19'-3" | 17'-11" | 17'-10" | 16'-7" |
|  |  | 230 | 23'-5" | 21'-9" | 22'-0" | 20'-5" | 19'-11" | 18'-6" | 18'-5" | 17'-2" |
|  |  | 360 | 24'-11" | 23'-2" | 23'-5" | 21'-9" | 21'-2" | 19'-8" | 19'-7" | 18'-3" |
|  |  | 560 | 28'-9" | 26'-8" | 26'-11" | 25'-0" | 24'-4" | 22'-8" | 22'-6" | 21'-0" |
|  | 14" | 110 | 24'-6" | 22'-9" | 23'-0" | 21-4" | 20'-10" | 19'-4" | 19'-3" | 17'-11" |
|  |  | 210 | 25'-10" | 24'-0" | 24'-3" | 22'-6" | 21'-11" | 20'-5" | 20'-4" | 18'-11" |
|  |  | 230 | 26'-8" | 24'-9" | 25'-1" | 23'-3" | 22'-8" | 21'-1" | 20'-11" | 19'-6" |
|  |  | 360 | 28'-4" | 26'-4" | 26'-7" | 24'-9" | 24'-1" | 22'-5" | 22'-3" | 20'-9" |
|  |  | 560 | 32'-7" | 30'-3" | 30'-7" | 28'-5" | 27'-8" | 25'-9" | 25'-7" | 23'-10" |
|  | 16" | 210 | 28'-8" | 26'-7" | 26'-11" | 25'-0" | 24'-4" | 22'-8" | 21'-6" | 20'-11" |
|  |  | 230 | 29'-7" | 27'-5" | 27'-9" | 25'-9" | 25'-1" | 23'-4" | 23'-3" | 21'-7" |
|  |  | 360 | 31'-5" | 29'-2" | 29'-6" | 27'-5" | 26'-8" | 24'-10" | 24'-8" | 22'-11" |
|  |  | 560 | $36^{\prime}-1{ }^{\prime \prime}$ | 33'-6" | 33'-10" | 31'-5" | 30'-8" | 28'-6" | 28'-4" | $26^{\prime}-4{ }^{\prime \prime}$ |
| 19.2" | 91⁄2" | 110 | 16'-11" | $15^{\prime}-8{ }^{\prime \prime}$ | 15'-10" | 14'-9" | 14'-4" | 13'-4" | 13'-3" | 12'-4" |
|  |  | 210 | 17'-10" | $16^{\prime}-7{ }^{\prime \prime}$ | 16'-9" | 15'-7" | 15'-2" | 14'-1" | 14'-0" | 13'-0" |
|  |  | 230 | 18'-6" | 17'-2" | 17'-4" | 16'-1" | 15'-8" | 14'-7" | 14'-5" | 13'-6" |
|  |  | 360 | 19'-8" | 18'-3" | 18'-5" | 17-2" | $16^{\prime}-8{ }^{\prime \prime}$ | $15^{\prime}-6{ }^{\prime \prime}$ | $15^{\prime}-4{ }^{\prime \prime}$ | 14'-4" |
|  |  | 560 | 22'-7" | 21'-0" | 21'-3" | 19'-9" | 19'-2" | 17'-10" | 17'-8" | 16'-6" |
|  | 117/8" | 110 | 20'-2" | 18'-9" | 18'-11" | 17'-7" | 17'-2" | 15'-11" | 15'-10" | 14'-9" |
|  |  | 210 | 21'-4" | 19'-10" | 20'-0" | 18'-7" | 18'-1" | $16^{\prime}-10^{\prime \prime}$ | 16'-9" | 15'-7" |
|  |  | 230 | 22'-0" | 20'-5" | 20'-8" | 19'-2" | 18'-8" | 17'-4" | 17'-3" | 16'-1" |
|  |  | 360 | 23'-5" | 21'-9" | 22'-0" | 20'-5" | 19'-10" | 18'-6" | 18'-4" | 17'-1" |
|  |  | 560 | 26'-11" | 25'-0" | 25'-3" | 23'-6" | 22'-10" | 21'-3" | 21'-1' | 19'-8" |
|  | 14" | 110 | 22'-11" | $21^{\prime}-4{ }^{\prime \prime}$ | 21'-7" | 20'-0" | 19'-3" | 18'-2" | $16^{\prime}-2{ }^{\prime \prime}$ | 16'-9" |
|  |  | 210 | 24'-3" | 22'-6" | 22'-9" | 21'-2" | 20'-7" | 19'-2" | 17'-11" | 17-9" |
|  |  | 230 | 25'-1" | 23'-3" | 23'6" | 21'-10" | 21'-3" | 19'-9" | 19'-8" | 18'-4" |
|  |  | 360 | 26'-7" | 24'-9" | 25'-0" | 23'-3" | 22'-7" | 21'-0" | 20'-7" | 19'-5" |
|  |  | 560 | $30^{\prime}-7{ }^{\prime \prime}$ | 28'-5" | 28'-8" | 26'-8" | 25'-11" | $24^{\prime}-2{ }^{\prime \prime}$ | 24'-0" | 22'-4" |
|  | 16" | 210 | 26'-11" | 25'-0" | 25'-3" | 23'-6" | 21'-4" | 21'-3" | 17'-11" | 19'-4" |
|  |  | 230 | 27'-9" | 25'-9" | 26'-1" | 24'-3" | 23'-7" | 21'-11" | 20'-1" | 20'-3" |
|  |  | 360 | 29'-6" | 27'-5" | 27'-8" | 25'-9" | 24'-6" | 23'-3" | 20'-7" | 20'-10" |
|  |  | 560 | 33'-10" | $31^{\prime}-5^{\prime \prime}$ | 31'-9" | 29'-6" | 28'-9" | 26'-9" | 25'-1" | 24'-5" |
| 24" | 91⁄2" | 110 | 15'-7" | 14'-6" | 14'-8" | 13'-7" | 13'-3" | 12'-4" | 12'-3" | 11'-5" |
|  |  | 210 | 16'-6" | 15'-4" | 15'-6" | 14'-5" | 14'-0" | $13^{\prime}-0{ }^{\prime \prime}$ | 12'-11" | 12'-0" |
|  |  | 230 | 17'-1' | 15'-10" | 16'-0" | 14'-11" | 14'-5" | 13'-6" | $13^{\prime}-4 "$ | 12'-5" |
|  |  | 360 | 18'-2" | 16'-11" | 17'-0" | 15'-10" | 15'-4" | 14'-4" | 14'-2" | 13'-3" |
|  |  | 560 | 20'-11" | 19'-5" | 19'-7" | 18'-3" | 17'-8" | 16'-6" | $16^{\prime}-4 "$ | 15'-3" |
|  | 117/8" | 110 | 18'-8" | 17'-4" | 17'-6" | 16'-4" | 15'-4" | 14'-9" | 12'-11" | 13'-8" |
|  |  | 210 | 19'-9" | 18'-4" | 18'-6" | 17'-3" | 16'-9" | 15'-7" | 14'-4" | 14'-5" |
|  |  | 230 | 20'-4" | 18'-11" | 19'-1" | 17'-9" | 17'-3" | 16'-1" | 15'-11" | 14'-10" |
|  |  | 360 | 21'-8" | 20'-2" | 20'4" | 18'-11" | 18'-4" | 17'-1" | $16^{\prime}-5{ }^{\prime \prime}$ | 15'-10" |
|  |  | 560 | 24'-11" | 23'-2" | 23'-5" | 21'-9" | 21'-1" | 19'-8" | 19'-6" | 18'-2" |
|  | 14" | 110 | 20'-6" | 19'-7" | 19'-0" | 18'-6" | 15'-4" | $16^{\prime}-5{ }^{\prime \prime}$ | 12'-11" | 14'-0" |
|  |  | 210 | 22'-5" | 20'-10" | 21'1" | 19'-7" | 17'-1' | 17'-9" | 14'-4" | 15'-6" |
|  |  | 230 | 23'-2" | 21'-6" | 21'-9" | 20'-3" | 19'-2" | 18'-4" | 16'-1" | 16'-4" |
|  |  | 360 | 24'-7" | 22'-11" | 23'-1" | 21'-6" | 19'-7" | 19'-5" | 16'-5" | 16'-8" |
|  |  | 560 | 28'-4" | 26'-4" | 26'-7" | 24'-8" | 23'-11" | 22'-4" | 20'-1" | 19'-6" |
|  | 16" | 210 | 23'-11" | 23'-0" | 21-1" | 21'-9" | 17'-1" | 18'-2" | 14'-4" | 15'-6" |
|  |  | 230 | 25'-4" | 23'-11" | 23'-8" | 22'-5" | 19'-2" | 19'-3" | 16'-1' | 16'-4" |
|  |  | 360 | 27'-3" | 25'-4" | 24'-3" | 23'-8" | 19'-7" | 19'-7" | 16'-5" | 16'-8" |
|  |  | 560 | $31^{\prime}-4{ }^{\prime \prime}$ | 29'-1" | 29'-5" | 27'-4" | 23'-11" | 22'-11" | 20'-1" | 19'-6" |

## How to Use This Table

1. Determine appropriate unfactored snow and dead load.
2. If your slope is $6: 12$ or less, use the Low slope column. If it is between 6:12 and $12: 12$, use the High column.
3. Scan down the column until you find a span that meets or exceeds the span of your application.
4. Select $\mathrm{TJI}{ }^{\circledR}$ joist and on-centre spacing.

## General Notes

- Table is based on:
- Minimum bearing length of $13 / 4$ " end and $31 / 2$ " intermediate, without web stiffeners.
- Uniform loads.
- More restrictive of simple or continuous span.
- Minimum roof slope of $1 / 4: 12$.
- Unfactored total load joist deflection limited to L/180.
- Unfactored live load joist deflection limited to L/360.
- For continuous spans, ratio of short span to long span should be 0.4 or greater to prevent uplift.
- A support beam or wall at the high end is required. Ridge board applications do not provide adequate support.
- For flat roofs or other loading conditions not shown, refer to Weyerhaeuser software.


## Roof-Factored Resistance, Standard Term (PLF)

| Depth | TJ® | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance <br> Total Load | Unfactored Deflection Resistance |  | Factored Strength Resistance <br> Total <br> Load |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Live } \\ & \text { Load } \\ & \text { L/360 } \end{aligned}$ | Total Load L/180 | Total Load | $\begin{aligned} & \text { Live } \\ & \text { Load } \\ & \text { L/360 } \end{aligned}$ | Total Load L/180 | Total Load | Live Load L/360 | Total Load L/180 | Total Load | $\begin{aligned} & \text { Live } \\ & \text { Load } \\ & \text { L/360 } \end{aligned}$ | Total Load L/180 |  | $\begin{aligned} & \text { Live } \\ & \text { Load } \\ & \text { L/360 } \end{aligned}$ | Total Load L/180 |  |
|  |  | Roof Joist Horizontal Clear Span |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | $8^{1}$ |  |  | $10^{1}$ |  |  | 12' |  |  | $14^{\prime}$ |  |  | $16^{1}$ |  |  |
| 91/2" | 110 | * | * | 300 | * | * | 240 | 114 | * | 201 | 74 | * | 166 | 51 | * | 127 |
|  | 210 | * | * | 332 | * | * | 266 | 132 | * | 222 | 87 | * | 191 | 60 | * | 153 |
|  | 230 | * | * | 373 | * | * | 299 | 145 | * | 250 | 95 | * | 214 | 66 | * | 170 |
|  | 360 | * | * | 381 | * | * | 306 | 170 | * | 255 | 112 | * | 219 | 78 | * | 192 |
|  | 560 | * | * | 465 | * | * | 373 | * | * | 311 | 164 | * | 267 | 115 | * | 234 |
| 117/8" | 110 | * | * | 300 | * | * | 240 | * | * | 201 | * | * | 172 | 85 | * | 151 |
|  | 210 | * | * | 332 | * | * | 266 | * | * | 222 | * | * | 191 | 98 | * | 167 |
|  | 230 | * | * | 373 | * | * | 299 | * | * | 250 | * | * | 214 | 107 | * | 188 |
|  | 360 | * | * | 381 | * | * | 306 | * | * | 255 | * | * | 219 | 127 | * | 192 |
|  | 560 | * | * | 465 | * | * | 373 | * | * | 311 | * | * | 267 | * | * | 234 |
| 14" | 110 | * | * | 300 | * | * | 240 | * | * | 201 | * | * | 172 | * | * | 151 |
|  | 210 | * | * | 332 | * | * | 266 | * | * | 222 | * | * | 191 | * | * | 167 |
|  | 230 | * | * | 373 | * | * | 299 | * | * | 250 | * | * | 214 | * | * | 188 |
|  | 360 | * | * | 381 | * | * | 306 | * | * | 255 | * | * | 219 | * | * | 192 |
|  | 560 | * | * | 465 | * | * | 373 | * | * | 311 | * | * | 267 | * | * | 234 |
| 16" | 210 | * | * | 332 | * | * | 266 | * | * | 222 | * | * | 191 | * | * | 167 |
|  | 230 | * | * | 373 | * | * | 299 | * | * | 250 | * | * | 214 | * | * | 188 |
|  | 360 | * | * | 381 | * | * | 306 | * | * | 255 | * | * | 219 | * | * | 192 |
|  | 560 | * | * | 465 | * | * | 373 | * | * | 311 | * | * | 267 | * | * | 234 |
|  |  | $18^{1}$ |  |  | $20^{\prime}$ |  |  | 22' |  |  | $24^{\prime}$ |  |  | $26^{1}$ |  |  |
| 91/2" | 110 | 36 | * | 101 | 27 | 54 | 81 |  |  |  |  |  |  |  |  |  |
|  | 210 | 43 | * | 121 | 31 | 63 | 98 | 24 | 48 | 81 |  |  |  |  |  |  |
|  | 230 | 47 | * | 134 | 35 | 70 | 109 | 26 | 53 | 90 | 20 | 41 | 76 |  |  |  |
|  | 360 | 56 | 112 | 171 | 41 | 83 | 154 | 31 | 63 | 129 | 24 | 49 | 109 | 19 | 39 | 93 |
|  | 560 | 83 | * | 208 | 62 | 124 | 188 | 47 | 95 | 171 | 37 | 74 | 156 | 29 | 59 | 143 |
| 117/8" | 110 | 61 | * | 127 | 45 | * | 103 | 34 | * | 85 |  |  |  |  |  |  |
|  | 210 | 71 | * | 149 | 52 | * | 124 | 40 | * | 102 | 31 | * | 86 |  |  |  |
|  | 230 | 77 | * | 167 | 57 | * | 138 | 44 | * | 114 | 34 | * | 96 | 27 | 54 | 82 |
|  | 360 | 92 | * | 171 | 68 | * | 154 | 52 | * | 140 | 41 | 82 | 128 | 32 | 65 | 118 |
|  | 560 | 135 | * | 208 | 101 | * | 188 | 78 | * | 171 | 61 | * | 156 | 48 | 97 | 144 |
| 14" | 110 | 88 | * | 134 | 65 | * | 121 | 50 | * | 101 | 39 | * | 85 |  |  |  |
|  | 210 | 102 | * | 149 | 76 | * | 134 | 58 | * | 121 | 45 | * | 102 | 36 | * | 87 |
|  | 230 | 111 | * | 167 | 83 | * | 150 | 63 | * | 135 | 49 | * | 113 | 39 | * | 97 |
|  | 360 | * | * | 171 | 98 | * | 154 | 75 | * | 140 | 59 | * | 128 | 47 | * | 118 |
|  | 560 | * | * | 208 |  | * | 188 | 111 | * | 171 | 87 | * | 156 | 69 | * | 144 |
| $16 "$ | 210 | * | * | 149 | * | * | 134 | 78 | * | 122 | 61 | * | 112 | 48 | * | 100 |
|  | 230 | * | * | 167 | * | * | 150 | 85 | * | 137 | 66 | * | 125 | 53 | * | 111 |
|  | 360 | * | * | 171 | * | * | 154 |  | * | 140 | 79 | * | 128 | 63 | * | 118 |
|  | 560 | * | * | 208 | * | * | 188 | * | * | 171 | - | * | 156 | 92 | * | 144 |

* Indicates value does not control.


## How to Use These Tables

1. Calculate actual factored total load and unfactored snow and total load on the joist in pounds per linear foot (plf).
2. Select appropriate Roof Joist Horizontal Clear Span. For slopes greater than 2:12, approximate the increased dead load by multiplying the joist horizontal clear span by the Slope Factor shown on page 33
3. Scan down the columns to find a TJI® joist that meets or exceeds the actual unfactored snow and total loads, and the factored total load. All three columns must be checked.

## General Notes

- Tables are based on:
- Minimum bearing length of $13 / 4^{\prime \prime}$ end and $31 / 2^{\prime \prime}$ intermediate, without web stiffeners
- Uniform loads.
- More restrictive of simple or continuous span.
- Minimum roof slope of $1 / 4: 12$.
- No composite action provided by sheathing.


| Depth | TJ® | Single Joist-Top Mount |  |  |  | Single Joist-Face Mount |  |  |  | Face Mount Skewed $45^{\circ}$ Joist Hanger |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |  |  | Header | Joist |
| 91/2" | 110 | ITS1.81/9,5 | 1,540 | 10d | N.A. | IUS1.81/9.5 | 1,540 | 10d | N.A. | SUR/L1.81/9 | 1,925 | 16d | 10d x 11/2" |
|  | 210 | ITS2.06/9.5 | 1,690 | 10d | N.A. | IUS2.06/9.5 | 1,690 | 10d | N.A. | SUR/L2.1/9 | 2,100 | 16d | 10d x 11/2" |
|  | 230 | ITS2.37/9.5 | 1,690 | 10d | N.A. | IUS2.37/9.5 | 1,690 | 10d | N.A. | SUR/L2.37/9 | 2,100 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 360 | ITS2.37/9.5 | 1,690 | 10d | N.A. | IUS2.37/9.5 | 1,690 | 10d | N.A. | SUR/L2.37/9 | 2,250 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{1¹/2"}$ |
|  | 560 | ITS3.56/9.5 | 1,690 | 10d | N.A. | IUS3.56/9.5 | 1,685 | 10d | N.A. | SUR/L410 | 2,360 | 16d | 16d |
| 111/8" | 110 | ITS1.81/11.88 | 1,540 | 10d | N.A. | IUS1.81/11.88 | 1,540 | 10d | N.A. | SUR/L1.81/11 | 1,960 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\text {" }}$ |
|  | 210 | ITS2.06/11.88 | 1,690 | 10d | N.A. | IUS2.06/11.88 | 1,690 | 10d | N.A. | SUR/L2.1/11 | 2,175 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 230 | ITS2.37/11.88 | 1,690 | 10d | N.A. | IUS2.37/11.88 | 1,770 | 10d | N.A. | SUR/L2.37/11 | 2,225 | 16d | 10d x 11/2" |
|  | 360 | ITS2.37/11.88 | 1,690 | 10d | N.A. | IUS2.37/11.88 | 1,805 | 10d | N.A. | SUR/L2.37/11 | 2,260 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 560 | ITS3.56/11.88 | 1,690 | 10d | N.A. | IUS3.56/11.88 | 1,685 | 10d | N.A. | SUR/L410 | 2,360 | 16d | 16d |
| 14" | 110 | ITS1.81/14 | 1,540 | 10d | N.A. | IUS1.81/14 | 1,540 | 10d | N.A. | SUR/L1.81/14 | 1,960 | 16d | 10d x 11/2" |
|  | 210 | ITS2.06/14 | 1,690 | 10d | N.A. | IUS2.06/14 | 1,690 | 10d | N.A. | SUR/L2.1/14 | 2,175 | 16d | $10 \mathrm{~d} \times 1$ 1/2" |
|  | 230 | ITS2.37/14 | 1,690 | 10d | N.A. | IUS2.37/14 | 1,770 | 10d | N.A. | SUR/L2.37/14 | 2,225 | 16d | $10 \mathrm{~d} \times 1$ 1/2" |
|  | 360 | ITS2.37/14 | 1,690 | 10d | N.A. | IUS2.37/14 | 1,805 | 10d | N.A. | SUR/L2.37/14 | 2,260 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{1} \mathrm{1/2"}$ |
|  | 560 | ITS3.56/14 | 1,690 | 10d | N.A. | IUS3.56/14 | 1,685 | 10d | N.A. | SUR/L414 | 2,360 | 16d | 16d |
| 16" | 210 | ITS2.06/16 | 1,690 | 10d | N.A. | IUS2.06/16 | 1,690 | 10d | N.A. | SUR/L2.1/14 | 2,175 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\text {" }}$ |
|  | 230 | ITS2.37/16 | 1,690 | 10d | N.A. | IUS2.37/16 | 1,770 | 10d | N.A. | SUR/L2.37/14 | 2,225 | 16d | $10 \mathrm{~d} \times 1$ 1/2" |
|  | 360 | ITS2.37/16 | 1,690 | 10d | N.A. | IUS2.37/16 | 1,805 | 10d | N.A. | SUR/L2.37/14 | 2,260 | 16 d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 560 | ITS3.56/16 | 1,690 | 10d | N.A. | IUS3.56/16 | 1,685 | 10d | N.A. | SUR/L414 | 2,360 | 16d | 16d |


| Depth | TJ ${ }^{\text {® }}$ | Double Joist-Top Mount |  |  |  | Double Joist-Face Mount |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) |  | iling | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |
| 91⁄2" | 110 | MIT49.5 | 2,420 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ | MIU3.56/9 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 210 | MIT4.28/9.5 | 2,420 | 16d | $10 \mathrm{dx} 11 / 2^{\prime \prime}$ | MIU4.28/9 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 230 | MIT359.5-2 | 2,420 | 16d | $10 \mathrm{dx} 11^{1 / 2}$ | MIU4.75/9 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 360 | MIT359.5-2 | 2,420 | 16d | $10 \mathrm{dx} 11 / 2^{\prime \prime}$ | MIU4.75/9 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 560 | HB7,12/9.5 | 5,270 | 16d | 16d | HU410-2 | 4,225 | 16d | 16d |
| 117/8" | 110 | MIT411.88 | 2,420 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ | MIU3.56/11 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2$ " |
|  | 210 | MIT4,28/11.88 | 2,420 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ | MIU4.28/11 | 3,230 | 16d | $10 \mathrm{dx} \times 1 / 2^{\prime \prime}$ |
|  | 230 | MIT3511.88-2 | 2,420 | 16d | 10d x 1112" | MIU4.75/11 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2 \mathrm{~L}$ |
|  | 360 | MIT3511.88-2 | 2,420 | 16d | 10d x 11⁄2" | MIU4.75/11 | 3,230 | 16d | $10 \mathrm{~d} \times 11 / 2$ " |
|  | 560 | HB7.12/11.88 | 5,450 | 16d | 16d | HU412-2 | 4,225 | 16d | 16 d |
| 14" | 110 | MIT414 | 2,420 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ | MIU3.56/14 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 210 | MIT4.28/14 | 2,420 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ | MIU4.28/14 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 21$ |
|  | 230 | MIT3514-2 | 2,420 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ | MIU4.75/14 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 2{ }^{\prime \prime}$ |
|  | 360 | MIT3514-2 | 2,420 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | MIU4.75/14 | 3,485 | 16d | 10d x 1½" |
|  | 560 | HB7.12/14 | 5,450 | 16d | 16d | HU414-2 | 4,615 | 16d | 16d |
| 16" | 210 | BA4.28/16 | 4,200 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | MIU4.28/16 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 2 \mathrm{~L}$ |
|  | 230 | MIT4.75/16 | 2,420 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | MIU4.75/16 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 21$ |
|  | 360 | MIT4.75/16 | 2,420 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | MIU4.75/16 | 3,485 | 16d | 10d x 1½" |
|  | 560 | HB7.12/16 | 5,450 | 16d | 16d | HU414-2 | 4,615 | 16d | 16d |


| TJ ${ }^{\text {® }}$ | Variable Slope Seat Joist Hanger ${ }^{(1)}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hanger | Fac. Res. (lbs) |  | Nailing |  |
|  |  | Sloped Only | Sloped and Skewed | Header | Joist |
| 110 | LSSR1.812 | 1,485 | 1,200 | 10d | 10d x 11/2" |
| 210 | LSSR2.1Z | 1,560 | 1,200 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 230 | LSSR2.372 | 1,560 | 1,200 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 360 | LSSR2.37Z | 1,560 | 1,200 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 560 | LSSR410Z | 2,045 | 1,835 | 16d | 16d |

## General Notes

Bold italic hangers require web stiffeners.
Factored resistances will vary with different nailing criteria or other support conditions; contact your Weyerhaeuser representative for assistance.

- Hanger factored resistances shown are either joist bearing or hanger factored resistance-whichever is less. Joist end reaction must be checked to ensure it does not exceed the factored resistance shown in the tables.
- All factored resistances are for downward loads, standard term.
- Fill all round, dimple, and positive-angle nail holes.
- Use sloped seat hangers and beveled web stiffeners when $T J{ }^{®}$ joist slope exceeds $1 / 4: 12$.
- Leave $1 / 16^{\prime \prime}$ clearance ( $1 / 8^{\prime \prime}$ maximum) between the end of the supported joist and the header or hanger.
- Nails: $16 \mathrm{~d}=0.162^{\prime \prime} \times 3 ½ 2^{\prime \prime}, 10 \mathrm{~d}=0.148^{\prime \prime} \times 3^{\prime \prime}$, and $10 \mathrm{~d} \times 11 / 2^{\prime \prime}=0.148^{\prime \prime} \times 11 / 2^{\prime \prime}$.


## Support Requirements

- Support material assumed to be Trus Joist ${ }^{\circledR}$ engineered lumber or sawn lumber (Douglas fir, southern pine, or spruce-pine-fir species).
- Minimum support width for single- and double-joist top mount hangers is $3^{\prime \prime}$ ( $1^{1 ⁄ 2} 2^{\prime \prime}$ for ITS hangers).
- Minimum support width for face mount hangers with 10 d and 16 d nails (clinched) is $1 \frac{1}{2} 2^{\prime \prime}$ and $13 / 4^{\prime \prime}$, respectively.


Single Joist, Top Mount


Single Joist, Face Mount


Face Mount Skewed $45^{\circ}$ Joist Hanger


Double Joist, Top Mount


Double Joist, Face Mount


Variable Slope Seat Joist Hanger


Variable Slope Seat Connector

| Depth | TJ ${ }^{\text {® }}$ | Single Joist-Top Mount |  |  |  | Single Joist-Face Mount |  |  |  | Face Mount Skewed $45^{\circ}$ Joist Hanger |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |  |  | Header | Joist |
| 91/2" | 110 | TH017950 | 1,540 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2 \mathrm{~L}$ | IHFL17925 | 1,750 | 10d | N.A. | SKH1720L/R | 1,485 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 210 | TFL2095 | 1,690 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 22^{\prime \prime}$ | IHFL20925 | 1,895 | 10d | N.A. | SKH2020L/R | 1,640 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 230 | TFL2395 | 1,770 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL23925 | 1,960 | 10d | N.A. | SKH2320L/R | 1,720 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 360 | TFL2395 | 1,805 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL23925 | 1,995 | 10d | N.A. | SKH2320L/R | 1,755 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11⁄2"}$ |
|  | 560 | TH035950 | 2,255 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL35925 | 2,305 | 10d | N.A. | SKH410L/R ${ }^{(3)}$ | 2,305 | 16d | 16d |
| 111/8" | 110 | TH017118 | 1,540 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL17112 | 1,750 | 10d | N.A. | SKH1720L/R | 1,485 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 210 | TFL20118 | 1,690 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL20112 | 1,895 | 10d | N.A. | SKH2020L/R | 1,640 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 230 | TFL23118 | 1,770 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL23112 | 1,960 | 10d | N.A. | SKH2320L/R | 1,720 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 360 | TFL23118 | 1,805 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | IHFL23112 | 1,995 | 10d | N.A. | SKH2320L/R | 1,755 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 560 | TH035118 | 2,255 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | IHFL35112 | 2,305 | 10d | N.A. | SKH410L/R(3) | 2,305 | 16d | 16d |
| 14" | 110 | TFL1714 | 1,540 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL1714 | 1,750 | 10d | N.A. | SKH1720L/R | 1,485 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 210 | TFL2014 | 1,690 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | IHFL2014 | 1,895 | 10d | N.A. | SKH2020L/R | 1,640 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 230 | TFL2314 | 1,770 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | IHFL2314 | 1,960 | 10d | N.A. | SKH2324L/R | 1,720 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 360 | TFL2314 | 1,805 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL2314 | 1,995 | 10d | N.A. | SKH2324L/R | 1,755 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 560 | TH035140 | 2,255 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL3514 | 2,305 | 10d | N.A. | SKH414L/R ${ }^{(3)}$ | 2,305 | 16d | 16d |
| $16^{\prime \prime}$ | 210 | TFL2016 | 1,690 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHFL2016 | 1,895 | 10d | N.A. | SKH2024L/R | 1,640 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 230 | TFL2316 | 1,770 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | IHFL2316 | 1,960 | 10d | N.A. | SKH2324L/R | 1,720 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 360 | TFL2316 | 1,805 | 10d | 10d x 1½" | IHFL2316 | 1,995 | 10d | N.A. | SKH2324L/R | 1,755 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
|  | 560 | TH035160 | 2,255 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 21$ | IHFL3516 | 2,305 | 10d | N.A. | SKH414L/R ${ }^{(3)}$ | 2,305 | 16d | 16d |


| Depth | TJ® | Double Joist-Top Mount |  |  |  | Double Joist-Face Mount |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |
| 91/2" | 110 | TH035950 | 2,620 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | IHF35925 | 3,310 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2 \mathrm{~L}$ |
|  | 210 | TH020950-2 | 3,320 | 16d | 10d | IHF20925-2 | 2,900 | 10d | 10d |
|  | 230 | TH023950-2 | 4,200 | 16d | 10d | IHF23925-2 | 2,900 | 10d | 10d |
|  | 360 | TH023950-2 | 4,375 | 16d | 10d | IHF23925-2 | 2,900 | 10d | 10d |
|  | 560 | BPH7195 | 4,340 | 16d | 10d | HD7100 | 4,180 | 16d | 16d |
| 111/8" | 110 | TH035118 | 2,620 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | IHF35112 | 3,310 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 210 | TH020118-2 | 3,355 | 16d | 10d | IHF20112-2 | 2,900 | 10d | 10d |
|  | 230 | TH023118-2 | 4,305 | 16d | 10d | THF23118-2 | 3,920 | 10d | 10d |
|  | 360 | TH023118-2 | 4,375 | 16d | 10d | THF23118-2 | 3,990 | 10d | 10d |
|  | 560 | BPH71118 | 4,305 | 16d | 10d | HD7120 | 4,180 | 16d | 16d |
| 14" | 110 | TH035140 | 3,385 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | IHF3514 | 3,310 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 210 | TH020140-2 | 3,355 | 16d | 10d | IHF2014-2 | 2,900 | 10d | 10d |
|  | 230 | TH023140-2 | 4,305 | 16d | 10d | THF23140-2 | 3,920 | 10d | 10d |
|  | 360 | TH023140-2 | 4,375 | 16d | 10d | THF23140-2 | 3,990 | 10d | 10d |
|  | 560 | BPH7114 | 4,305 | 16d | 10d | HD7140 | 4,180 | 16d | 16d |
| 16" | 210 | TH020160-2 | 3,355 | 16d | 10d | IHF2014-2 | 2,900 | 10d | 10d |
|  | 230 | TH023160-2 | 4,305 | 16d | 10d | THF23160-2 | 3,920 | 10d | 10d |
|  | 360 | TH023160-2 | 4,375 | 16d | 10d | THF23160-2 | 3,990 | 10d | 10d |
|  | 560 | BPH7116 | 4,305 | 16d | 10d | HD7140 | 4,180 | 16d | 16d |


| TJ ${ }^{\text {® }}$ | Variable Slope Seat Joist Hanger ${ }^{(1)}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hanger | Fac. Res. (lbs) |  | Nailing |  |
|  |  | Sloped Only | Sloped and Skewed | Header | Joist |
| 110 | LSSH179 | 1,925 | 1,925 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 210 | LSSH2O | 1,990 | 1,990 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 230 | LSSH23 | 1,990 | 1,990 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 360 | LSSH23 | 1,990 | 1,990 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 560 | LSSH35 | 2,515 | 2,390 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |


| TJ® | Variable Slope Seat Connector ${ }^{(4)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  | Header | Joist |
| 110 | TMP175 | 1,270 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | TMPH175 | 1,925 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 210 | TMP21 | 1,425 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 22^{\prime \prime}$ |
|  | TMPH21 | 2,100 | 10d | $10 \mathrm{dx} \mathrm{11/2"}$ |
| 230 | TMP23 | 2,100 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 22^{\prime \prime}$ |
|  | TMPH23 | 2,100 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2 \mathrm{~L}$ |
| 360 | TMP23 | 2,175 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | TMPH23 | 2,250 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 560 | TMP4 | 2,175 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | TMPH4 | 2,635 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |

Table footnotes for pages 14 and 15 :
(1) LSSR and LSSH hangers can be field adjusted for slopes and skews of up to 45 degrees. Additional lateral restraints are required for 16 " deep $\mathrm{TJI®}$ joists
(2) VPA connectors are allowed on slopes of 3:12 through 12:12 only.
(3) Miter cut is required at end of joist.
(4) TMP connectors are allowed on slopes of 1:12 through 6:12 only, and TMPH connectors are allowed on slopes of 6:12 through 12:12 only.

Also see General Notes on page 14.


Table A—End Support (Minimum distance from edge of hole to inside face of nearest end support)

| Depth | TJ® | Round Hole Size |  |  |  |  |  |  |  |  | Square or Rectangular Hole Size |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $2^{\prime \prime}$ | $3 "$ | $4 "$ | $5{ }^{\prime \prime}$ | $61 / 2^{\prime \prime}$ | 7" | 87/8" | 11" | 13 " | $2^{\prime \prime}$ | 3" | $4{ }^{\text {" }}$ | $5{ }^{\prime \prime}$ | 61/2" | $7{ }^{7}$ | 87/8" | $11 "$ | 13" |
| 91/2" | 110 | $1^{1}-0 /$ | $1^{1}-6{ }^{\prime \prime}$ | 2'-0" | 3'-0" | $5{ }^{\prime}-0{ }^{\prime \prime}$ |  |  |  |  | 1'-0" | 1'-6" | 2'-6" | $3^{\prime \prime}-6{ }^{\prime \prime}$ | $4^{\prime}-6{ }^{\prime \prime}$ |  |  |  |  |
|  | 210 | 1'-0" | $1^{1}-6{ }^{\prime \prime}$ | 2'-6" | $3^{\prime}-0{ }^{\prime \prime}$ | 5'-6" |  |  |  |  | 1'-0" | 2'-0" | 2'-6" | $4^{\prime}-0{ }^{\prime \prime}$ | 5'-0" |  |  |  |  |
|  | 230 | 1'-6" | 2'-0" | 2'-6" | 3'-6" | 5'-6" |  |  |  |  | 1'-0" | 2'-0" | 3'-0" | $4^{\prime}-6 "$ | 5'-0" |  |  |  |  |
|  | 360 | 1'-6" | 2'-0" | 3'-0" | 4'-0" | $6^{\prime}-0{ }^{\prime \prime}$ |  |  |  |  | 1'-6" | 2'-6" | $3^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-0{ }^{\prime \prime}$ | 5'-6" |  |  |  |  |
|  | 560 | $1^{1}$-6" | 2'-6" | $3^{\prime}-6{ }^{\prime \prime}$ | 5'-0" | 7'-0" |  |  |  |  | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | $4^{\prime}-0 \mid$ | $5^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ |  |  |  |  |
| 111/8" | 110 | 1'-0" | $1^{\prime}-0 \mid$ | 1'-6" | 2'-0" | 2'-6" | 3'-0" | 5'-6" |  |  | 1'-0" | 1'-6" | 2'-0" | 2'-6" | 4'-6" | 5'-0" | $6^{\prime}-0{ }^{\prime \prime}$ |  |  |
|  | 210 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-6{ }^{\prime \prime}$ | $2^{\prime}-0^{\prime \prime}$ | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ |  |  | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-6{ }^{\prime \prime}$ | 2'-6" | $3^{\prime}-0{ }^{\prime \prime}$ | $5^{\prime}-0{ }^{\prime \prime}$ | 5'-6" | $6^{\prime}-6{ }^{\prime \prime}$ |  |  |
|  | 230 | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-6{ }^{\prime \prime}$ | 2'-0" | 2'-6" | 3'-0" | 3'-6" | $6^{\prime}-6{ }^{\prime \prime}$ |  |  | 1'-0" | 2'-0" | 2'-6" | $3^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-6{ }^{\prime \prime}$ | 5'-6" | 7'-0" |  |  |
|  | 360 | $1^{1}$-6" | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | 3'-6" | 4'-6" | 5'-0" | 7'-0" |  |  | 1'-6" | 2'-6" | 3'-6" | $4^{\prime}-6{ }^{\prime \prime}$ | 6'-6" | 6'-6" | 7'-6" |  |  |
|  | 560 | $1^{1}-6{ }^{\prime \prime}$ | 2'-6" | $3^{\prime}-0{ }^{\prime \prime}$ | $4{ }^{\prime}-0{ }^{\prime \prime}$ | 5'-6" | 6'-0" | 8'-0" |  |  | 2'-6" | $3^{\prime}-6{ }^{\prime \prime}$ | $4^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-6{ }^{\prime \prime}$ | 7'-0" | 7'-6" | 8'-0" |  |  |
| $14 "$ | 110 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | 1'-0" | 1'-6" | 2'-0" | $3^{\prime}-0 / 1$ | $5^{\prime}-6{ }^{\prime \prime}$ |  | 1'-0" | $1^{\prime}-0 \mid$ | $1^{1}-6{ }^{\prime \prime}$ | $2^{\prime}-0 \mid$ | 3'-6" | 4'-0" | $6^{\prime}-0{ }^{\prime \prime}$ | 8'-0" |  |
|  | 210 | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | 1'-0" | $1^{1}-6{ }^{\prime \prime}$ | 2'-0" | 2'-6" | 3'-6" | $6^{\prime}-0{ }^{\prime \prime}$ |  | 1'-0" | 1'-0" | 2'-0" | 2'-6" | $4^{\prime}-0{ }^{\prime \prime}$ | 4'-6" | $6^{\prime}-6{ }^{\prime \prime}$ | 8'-6" |  |
|  | 230 | 1'-0" | $1^{1}-0{ }^{\prime \prime}$ | 1'-0" | $1^{1}-6{ }^{\prime \prime}$ | 2'-6" | 2'-6" | $4^{\prime}-0{ }^{\prime \prime}$ | 7'-0" |  | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | 4'-0" | 5'-0" | 7'-0" | $9^{\prime}-0{ }^{\prime \prime}$ |  |
|  | 360 | 1'-0" | $1^{1}-0{ }^{\prime \prime}$ | 1'-6" | 2'-6" | 3'-6" | 4'-0" | 5'-6" | $8^{\prime}-0{ }^{\prime \prime}$ |  | 1'-0" | 1'-6" | $2^{2}-6{ }^{\prime \prime}$ | $4^{\prime}-0 \mid$ | $6^{\prime}-0{ }^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | 8'-0" | 9'-6" |  |
|  | 560 | $1^{1}$-0" | $1^{1}-0{ }^{\prime \prime}$ | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | 4'-6" | $5^{\prime}-0^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | $9^{\prime}-011$ |  | 1'-6" | $3^{\prime}-0{ }^{\prime \prime}$ | $4^{\prime}-0{ }^{\prime \prime}$ | $5^{\prime}-0{ }^{\prime \prime}$ | 7'-0" | 7'-6" | $9^{\prime}-01$ | 10'-0" |  |
| 16" | 210 | $1^{1}-0 /$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-0 \mid$ | $1^{1}-0 \mid$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-6{ }^{\prime \prime}$ | 2'-6" | $3^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\text {a }}$ | $1^{1}-0 \mid$ | $1^{1}-0{ }^{\prime \prime}$ | $2^{2}-0 /$ | $3^{\prime \prime}-01$ | $3^{1}-6{ }^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | $8^{\prime}-01$ | 11'-0" |
|  | 230 | 1'-0" | $1^{1}-0{ }^{\prime \prime}$ | 1'-0" | $1^{1}-0{ }^{\prime \prime}$ | 1'-6" | 1'-6" | $3^{\prime}-0{ }^{\prime \prime}$ | $4^{\prime}-0{ }^{\prime \prime}$ | 7'-0" | 1'-0" | $1^{\prime}-0 \mid$ | $1^{1}-0{ }^{\prime \prime}$ | $2^{\prime}-0 \mid$ | $3^{\prime}-6{ }^{\prime \prime}$ | 4'-0" | 7'-0" | 9'-0" | 11'-0" |
|  | 360 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | 2'-6" | 2'-6" | $4^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | $9^{\prime}-01$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-6{ }^{\prime \prime}$ | $3^{\prime}-0{ }^{\prime \prime}$ | $5^{\prime}-0 /$ | 5'-6" | 9'-0" | 10'-0" | 11'-6" |
|  | 560 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $2^{\prime}-6{ }^{\prime \prime}$ | $3^{\prime}-0{ }^{\prime \prime}$ | $5^{\prime}-0{ }^{\prime \prime}$ | $7^{1}-6{ }^{\prime \prime}$ | 10'-0" | 1'-0" | $2^{2}-0{ }^{\prime \prime}$ | $3^{\prime}-01$ | $4^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | 7'-0" | $10^{\prime}-0{ }^{\prime \prime}$ | 11'-0" | 12'-0" |

Table B—Intermediate or Cantilever Support
(Minimum distance from edge of hole to inside face of nearest intermediate or cantilever support)

| Depth | TJ® | Round Hole Size |  |  |  |  |  |  |  |  | Square or Rectangular Hole Size |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2" | 3" | 4" | $5{ }^{\prime \prime}$ | 61/2" | 7" | 87/8" | 11" | 13" | 2" | 3" | 4 " | $5{ }^{\prime \prime}$ | 61121 | 7" | 87/8" | 11" | 13" |
| 91/2" | 110 | 2'-0" | 2'-6" | 3'-6" | 4'-6" | 7'-6" |  |  |  |  | $1^{1}-6{ }^{\prime \prime}$ | $2^{\prime}-6{ }^{\prime \prime}$ | 3'-6" | 5'-6" | $6^{\prime}-6{ }^{\prime \prime}$ |  |  |  |  |
|  | 210 | 2'-0" | 2'-6" | 3'-6" | $5^{\prime}-0{ }^{\prime \prime}$ | 8'-0' |  |  |  |  | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | 4'-0" | $6^{\prime}-6{ }^{\prime \prime}$ | 7'-6" |  |  |  |  |
|  | 230 | 2'-6" | 3'-0" | 4'-0" | $5^{\prime}-6{ }^{\prime \prime}$ | 8'-6" |  |  |  |  | 2'-0" | $3^{\prime}-6{ }^{\prime \prime}$ | 4'-6" | $6^{\prime}-6{ }^{\prime \prime}$ | 7'-6" |  |  |  |  |
|  | 360 | $3^{\prime}-0^{\prime \prime}$ | 4'-0" | 5'-6" | $6^{\prime}-6^{\prime \prime}$ | $9^{\prime}-0{ }^{\prime \prime}$ |  |  |  |  | $3^{\prime}-0{ }^{\prime \prime}$ | $4^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-6{ }^{\prime \prime}$ | 7'-6" | 8'-0" |  |  |  |  |
|  | 560 | 3'-6" | 5'-0" | $6^{\prime}-0{ }^{\prime \prime}$ | 7'-6" | 10'-0" |  |  |  |  | 4'-0" | $5^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | $8^{\prime}-0{ }^{\prime \prime}$ | 9'-0" |  |  |  |  |
| 117/8" | 110 | $1^{1}-0{ }^{\prime \prime}$ | $1^{\prime \prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 2'-6" | 4'-0" | 4'-6" | 8'-6" |  |  | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 2'-6" | 4'-0" | 7'-0" | 7'-0" | 9'-6" |  |  |
|  | 210 | 1'-0" | 1'-0" | 2'-0" | $3^{\prime}-0{ }^{\prime \prime}$ | 4'-6" | 5'-0" | 9'-0" |  |  | 1'-0" | $2^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-0{ }^{\prime \prime}$ | 4'-6" | 8'-0" | 8'-0" | 10'-0" |  |  |
|  | 230 | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | 2'-6" | $3^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-0{ }^{\prime \prime}$ | 5'-6" | 10'-0" |  |  | $1^{\prime}-0{ }^{\prime \prime}$ | $2^{\prime}-6{ }^{\prime \prime}$ | 3'-6" | $5^{\prime}-0{ }^{\prime \prime}$ | 8'-6" | 9'-0" | 10'-6" |  |  |
|  | 360 | 2'-0" | 3'-0" | 4'-0" | $5^{\prime}-6{ }^{\prime \prime}$ | 7'-0" | 7'-6" | 11'-0" |  |  | 2'-0" | $3^{\prime}-6{ }^{\prime \prime}$ | 5'-0" | 7'-0" | 9'-6" | 9'-6" | $11^{\prime}-0{ }^{\prime \prime}$ |  |  |
|  | 560 | 1'-6" | 3'-0" | 4'-6" | 5'-6" | 8'-0" | 8'-6" | 12'-0" |  |  | 3'-0" | $4^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | 8'-0" | 10'-6" | 11'-0" | 12'-0" |  |  |
| 14" | 110 | $1^{1}-0{ }^{\prime \prime}$ | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | $2^{\prime}-6{ }^{\prime \prime}$ | 4'-6" | 8'-6" |  | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $2^{\prime}-6{ }^{\prime \prime}$ | 5'-0" | $6^{\prime}-0{ }^{\prime \prime}$ | 9'-0" | 12'-0" |  |
|  | 210 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-6" | $3^{\prime}-0{ }^{\prime \prime}$ | 5'-6" | 9'-6" |  | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | $3^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | 7'-0" | 10'-0" | $13^{\prime}-0^{\prime \prime}$ |  |
|  | 230 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $2^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-6{ }^{\prime \prime}$ | 4'-0" | $6^{\prime}-0{ }^{\prime \prime}$ | $10^{\prime}-6{ }^{\prime \prime}$ |  | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-6" | $4^{\prime}-0{ }^{\prime \prime}$ | 6'-6" | 7'-6" | $11^{\prime}-0{ }^{\prime \prime}$ | $13^{\prime}-6{ }^{\prime \prime}$ |  |
|  | 360 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | $3^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | 8'-6" | 12'-6" |  | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | 4'-0" | 5'-6" | 9'-0" | $10^{\prime}-0{ }^{\prime \prime}$ | 12'-0" | $14^{\prime}-0{ }^{\prime \prime}$ |  |
|  | 560 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | $3^{\prime}-6{ }^{\prime \prime}$ | $5^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-6{ }^{\prime \prime}$ | $9^{\prime}-6{ }^{\prime \prime}$ | $13^{\prime}-6^{\prime \prime}$ |  | $1^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-0{ }^{\prime \prime}$ | $5^{\prime}-0{ }^{\prime \prime}$ | $7^{\prime}-0^{\prime \prime}$ | $10^{\prime}-0^{\prime \prime}$ | $11^{\prime}-0^{\prime \prime}$ | $13^{\prime}-6{ }^{\prime \prime}$ | $15^{\prime}-0{ }^{\prime \prime}$ |  |
| $16 "$ | 210 | 1'-0" | $1^{\prime \prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 3'-6" | $6^{\prime}-0{ }^{\prime \prime}$ | 10'-0" | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 4'-6" | 5'-6" | $10^{\prime}-0{ }^{\prime \prime}$ | 12'-6" | $16^{\prime}-0{ }^{\prime \prime}$ |
|  | 230 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 2'-0" | 4'-0" | $6^{\prime}-6{ }^{\prime \prime}$ | 11'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-6" | 5'-0" | $6^{\prime}-0{ }^{\prime \prime}$ | 10'-6" | $13^{\prime}-6{ }^{\prime \prime}$ | 16'-6" |
|  | 360 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-0^{\prime \prime}$ | 4'-0" | $6^{\prime}-6{ }^{\prime \prime}$ | $10^{\prime}-0^{\prime \prime}$ | $13^{\prime}-6{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | 4'-0" | 7'-6" | 8'-6" | $13^{\prime}-0{ }^{\prime \prime}$ | $14^{\prime}-6{ }^{\prime \prime}$ | $17^{\prime}-0{ }^{\prime \prime}$ |
|  | 560 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $2^{\prime}-6{ }^{\prime \prime}$ | $3^{\prime}-6{ }^{\prime \prime}$ | 7'-0" | 11'-0" | 15'-0" | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 3'-6" | 5'-6" | 9'-0" | 10'-0" | 14'-6" | $16^{\prime}-0{ }^{\prime \prime}$ | $18^{\prime}-0{ }^{\prime \prime}$ |

- Rectangular holes based on measurement of longest side.


## General Notes

- Holes may be located vertically anywhere within the web. Leave $1 / 8$ " of web (minimum) at top and bottom of hole.
- Knockouts are located in web at approximately 12 " on-centre; they do not affect hole placement and may be located in the hatched zone.
- For simple span (5' minimum) uniformly loaded joists meeting the requirements of this guide, one maximum size round hole may be located at the centre of the joist span provided that no other holes occur in the joist.
- Distances are based on the maximum uniform loads shown in this guide. For other load conditions or hole configurations use ForteWEBTM software or contact your Weyerhaeuser representative.


This section contains design information for 18 "-24" deep Trus Joist ${ }^{\circledR}$ TJI ${ }^{\circledR}$ joists used in residential, multi-family, or light-commercial applications.
18 " and 20 " deep $\mathrm{TJ}^{\circledR}$ joists are readily available through your local Weyerhaeuser dealer or distributor. Offered with the flange sizes shown below, they come in lengths up to 60' (in 1' increments). 22" and 24" deep $\mathrm{TJI®}$ joists are only available in some regions; for more information, contact your Weyerhaeuser representative.

## Design Properties

| Depth | TJ® | JoistWeight (lbs/ft) | $\begin{gathered} \text { Joist Only } \\ \text { Elx } 100^{6} \\ \left(\text { (bs-in. }{ }^{2}\right) \end{gathered}$ | Factored Resistances-Standard Term |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | MaximumResistive Moment ${ }^{(1)}$ (ft-lbs) | Maximu Shear (lbs) | $13 / 4$ EndReaction (lbs) |  | $31 / 2$ " Intermediate Reaction (lbs) |  | 51⁄4" Intermediate Reaction (lbs) |  |
|  |  |  |  |  |  | No Web Stiffeners | With Web Stiffeners ${ }^{(2)}$ | No Web Stiffeners | With Web Stiffeners ${ }^{(2)}$ | No Web Stiffeners | With Web <br> Stiffeners <br> (2) |
| 18" | 360 | 3.7 | 1,085 | 15,745 | 3,830 | 1,705 | 2,225 | 3,885 | 4,400 | 4,740 | 5,255 |
| 18 | 560 | 4.8 | 1,631 | 24,205 | 4,785 | 1,995 | 2,680 | 4,735 | 5,425 | 5,455 | 6,140 |
| 20" | 360 | 4.0 | 1,376 | 17,485 | 4,200 | 1,705 | 2,225 | 3,885 | 4,400 | 4,740 | 5,255 |
| 20 | 560 | 5.1 | 2,064 | 26,890 | 5,280 | 1,995 | 2,680 | 4,735 | 5,425 | 5,455 | 6,140 |
| $22^{\prime \prime}$ | 560D | 5.6 | 2,606 | 30,060 | 5,690 | N.A. ${ }^{(3)}$ | 3,370 | N.A. ${ }^{(3)}$ | 7,255 | N.A. ${ }^{(3)}$ | 7,975 |
| 24" | 560D | 5.8 | 3,165 | 32,765 | 5,050 | N.A. ${ }^{(3)}$ | 3,370 | N.A. ${ }^{(3)}$ | 7,715 | N.A. ${ }^{(3)}$ | 8,430 |



TJ® 360 joists

TJI® 560 joists


TJ® ${ }^{(460 D ~ J o i s t ~}$




FLOOR SPAN TABLES

TJ॥® joists are intended Factored shear resistance may sometimes be increased at interior supports. For more information contact your Weyerhaeuser representative.

- The following formulas approximate the simple span uniform load deflection of $\Delta$ (inches):


## For TJI® 360 Joists

For TJI® 560 and 560D Joists

$$
\Delta=\frac{22.5 \mathrm{wL}^{4}}{\mathrm{El}}+\frac{2.67 \mathrm{wL}^{2}}{\mathrm{~d} \times 10^{5}}
$$

$\Delta=\frac{22.5 \mathrm{wL}^{4}}{\mathrm{El}}+\frac{2.29 \mathrm{wL}^{2}}{\mathrm{~d} \times 10^{5}}$
w = uniform load in pounds per linear foot
$L=$ span in feet
d = out-to-out depth of the joist in inches
$\mathrm{El}=$ value from table above

Some $\mathrm{JJ}^{\circledR}$ joist series may not be available in your region. Contact your Weyerhaeuser representative for information. for dry-use applications

5/8" OSB Subfloor (Glue-nailed)—Vibration-Controlled, Standard Term

| Depth | TJI ${ }^{\text {® }}$ | Directly Applied Ceiling |  |  |  | No Directly Applied Ceiling |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Simple or Continuous Span |  | Continuous Span Only |  | Simple or Continuous Span |  | Continuous Span Only |  |
|  |  | 16" o.c. | 19.2" o.c. | 16" o.c. | 19.2" 0.c. | 16" o.c. | 19.2" 0.c. | 16" o.c. | 19.2" o.c. |
| 40 PSF Live / 15 PSF Dead Load |  |  |  |  |  |  |  |  |  |
| 18" | 360 | 23'-2" | 22'-2" | 24'-6" | 23'-5' | 22'-4" | 21'-4" | 23'-7" | 22'-7" |
|  | 560 | 25'-4' | 24'-1' | 26'-9" | 25'-6' | 24'-6' | 23'-5' | 25'-11" | 24'-9" |
| 20" | 360 | 24'-9" | 23'-8" | 26'-3' | 25'-1'(1) | 23'-10" | 22'-9" | 25'-3" | 24'-1' |
|  | 560 | 27'-0' | 25'-9' | 28'-7' | 27'-3' | $26^{\prime}-3^{\prime \prime}$ | $25^{\prime}-0^{\prime \prime}$ | 27'-9' | 26'-5' |
| 22" | 560D | 28'-10'1 | 27'-6" | 30'-6" | 29'-1' | 28'-0' | 26'-8' | 29'-7' | 28'-2" |
| $24 "$ | 560D | $30^{\prime}-6{ }^{\prime \prime}$ | 29'-1' | 32'-3' | 30'-9' | 29'-6" | $28^{\prime}-1{ }^{\prime \prime}$ | 31'-3' | 29'-9' |
| 40 PSF Live Load / 30 PSF Dead Load |  |  |  |  |  |  |  |  |  |
| 18" | 360 | 23'-2" | 21'-9'1(1) | 24'-6'(1) | 22'-5'(1) | 22'-4" | 21'-4'(1) | 23'-7" | 22'-5'(1) |
|  | 560 | 25'-4' | 24'-1' | 26'-9' | $25^{\prime}-6^{\prime \prime}(1)$ | $24^{\prime}-6^{\prime \prime}$ | $23^{\prime}-5^{\prime \prime}$ | 25'-11' | 24'-9'(1) |
| 20" | 360 | 24'-9'1(1) | 21'-9'1(1) | 26'-3'(1) | 22'-5'(1) | 23'-10'(1) | 21'-9'(1) | 25'-3'11) | 22'-5'(1) |
|  | 560 | 27'-0" | $25^{\prime}-5^{\prime \prime}(1)$ | 28'-7" | 27'-3"(1) | $26^{\prime}-3^{\prime \prime}$ | $25^{\prime}-0^{\prime \prime}(1)$ | 27'-9" | $26^{\prime}-5^{\prime \prime}(1)$ |
| 22" | 560D | 28'-10" | 27'-6" | 30'-6" | 29'-1' | 28'-0' | 26'-8' | 29'-7" | 28'-2" |
| $24 "$ | 560D | $30^{\prime}-6{ }^{\prime \prime}$ | 29'-1' | 32'-3' | 30'-9' | $29^{\prime \prime}-6^{\prime \prime}$ | 28'-1' | 31'-3' | 29'-9' |

> To more accurately predict floor performance, use our TJ-Pro ${ }^{T M}$ Ratings
(1) Web stiffeners are required at intermediate supports of continuous-span joists when the intermediate bearing length is less than $51 / 4$ "and the span on either side of the intermediate bearing is greater than the following spans:

| 40 PSF Live Load/15 PSF Dead Load |  |  | 40 PSF Live Load / 30 PSF Dead Load |  |
| :---: | :---: | :---: | :---: | :---: |
| TJI® | $16^{\prime \prime}$ 0.c. | $19,2^{\prime \prime}$ o.c. | $16^{\prime \prime}$ o.c. | $19,2^{\prime \prime}$ o.c. |
| 360 | Not Required | $24^{\prime}-6^{\prime \prime}$ | $23^{\prime}-9{ }^{\prime \prime}$ | $19^{\prime}-9^{\prime \prime}$ |
| 560 |  |  | $24^{\prime}-2^{\prime \prime}$ |  |

- Bold italic spans indicate floors that would meet National Building Code of Canada (NBCC) vibration criteria but would be considered by $35 \%$ of the population to have marginal or unacceptable performance.


## 3/4" OSB Subfloor (Glue-nailed)—Vibration-Controlled, Standard Term

| Depth | TJI® | Directly Applied Ceiling |  |  |  |  |  | No Directly Applied Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Simple or Continuous Span |  |  | Continuous Span Only |  |  | Simple or Continuous Span |  |  | Continuous Span Only |  |  |
|  |  | 16" o.c. | 19.2" o.c. | 24" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 40 PSF Live / 15 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18" | 360 | 24'-8' | 23'-6" | 21'-6 ${ }^{\prime \prime}$ (1) | 26'-1' | 24'-10'11) | 22'-2'(1) | 23'-10' | 22'-8" | 21'-5'(1) | 25'-2' | 24'-0" | 22'-2'11) |
|  | 560 | 26'-10' | 25'-7' | 24'-2'11) | 28'-5' | 27'-0" | 25'-7'(1) | 26'-2' | 24'-10" | 23'-5' | 27'-8' | 26'-3' | 24'-10'(1) |
| 20" | 360 | 26'-4' | $25^{\prime}-1^{1 \prime}(1)$ | 21'-6 ${ }^{\prime \prime}$ (1) | 27'-10" | 26'-7'(1) | 22'-2'(1) | 25'-5" | 24'-3' | 21'-6'(1) | 26'-11' | 25'-7'(1) | 22'-2'11) |
|  | 560 | 28'-8' | 27'-4" | 25'-2'11) | $30^{\prime}-4{ }^{\prime \prime}$ | 28'-11' | 27'-3'(1) | 27'-11" | 26'-6' | $25^{\prime}-0^{\prime \prime}(1)$ | 29'-6" | 28'-1' | $26^{\prime}-6^{\prime \prime}(1)$ |
| 22" | 560D | 30'-7' | 29'-1' | 27'-6" | 32'-4' | 30'-10' | 29'-1' | 29'-9' | 28'-3' | 26'-8' | 31'-6" | 29'-11" | 28'-3" |
| 24 | 560D | 32'-4' | 30'-9' | 29'-0'1 | 34'-9'' | 32'-6" | 30'-9' | 31'-5" | 29'-10" | 28'-2' | $33^{\prime}-6{ }^{\prime \prime}$ | 31'-7" | 29'-9" |
| 40 PSF Live Load / 30 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18" | 360 | 24'-8'(1) | 21'-9'(1) | 17'-4'(1) | 26'-1"(1) | 22'-5'(1) | 17'-11'(1) | 23'-10'(1) | 21'-9'(1) | 17'-4'(1) | 25'-2"(1) | 22'-5"(1) | 17'-11'(1) |
|  | 560 | 26'-10' | 25'-5"(1) | 20'-4'(1) | 28'-5' | $27^{\prime}-0^{\prime \prime}(1)$ | $22^{\prime}-1{ }^{\prime \prime}(1)$ | 26'-2" | 24'-10'11) | 20'-4'(1) | 27'-8' | 26'-3"(1) | $22^{\prime}-1{ }^{1 \prime}(1)$ |
| 20" | 360 | 26'-1'(1) | 21'-9'(1) | 17'-4'(1) | $26^{\prime}-11^{\prime \prime}(1)$ | 22'-5"(1) | 17'-11'(1) | 25'-5"(1) | 21'-9'(1) | 17'-4'(1) | 26'-11'(1) | 22'-5'(1) | 17'-11'(1) |
|  | 560 | 28'-8' | 25'-5"(1) | 20'-4'11) | $30^{\prime}-4^{\prime \prime}(1)$ | 27'-8'(1) | 22'-1'1) | 27'-11" | 25'-5'(1) | 20'-4'(1) | 29'-6'11) | 27'-8"(1) | 22'-1'(1) |
| 22" | 560D | 30'-7' | 29'-1' | 27'-6" | 32'-4' | $30^{\prime}-10^{\prime \prime}$ | 29'-1' | 29'-9" | 28'-3' | 26'-8' | 31'-6" | 29'-11' | 28'-3" |
| 24" | 560D | 32'-4' | $30^{\prime}-9{ }^{\prime \prime}$ | 29'-0'1 | 34'-9' | 32'-6" | 30'-9' | 31'-5" | 29'-10" | 28'-2' | $33^{1}-6^{\prime \prime}$ | 31'-7' | 29'-9" |

## 7/8" OSB Subfloor (Glue-nailed)—Vibration-Controlled, Standard Term

| Depth | TJI® | Directly Applied Ceiling |  |  |  |  |  | No Directly Applied Ceiling |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Simple or Continuous Span |  |  | Continuous Span Only |  |  | Simple or Continuous Span |  |  | Continuous Span Only |  |  |
|  |  | 16" o.c. | 19.2" 0.c. | 24" o.c. | 16" o.c. | 19.2" 0.c. | 24" 0.c. | 16" o.c. | 19.2" 0.c. | 24" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 40 PSF Live / 15 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18" | 360 | 26'-0" | 24'-9"(1) | 21'-6"(1) | 27'-5" | 26'-2'(1) | 22'-2"(1) | 25'-2' | 23'-11" | 21'-6"(1) | 26'-7" | 25'-3"(1) | 22'-2'(1) |
|  | 560 | 28'-3' | 26'-11' | 25'-2'(1) | 29'-11" | 28'-5' | 26'-10'(1) | 27'-7' | $26^{\prime}-2{ }^{\prime \prime}$ | 24'-8'(1) | 29'-2" | 27'-8' | 26'-0'(1) |
| 20" | 360 | 27'-9" | 26'-6'(1) | 21'-6"(1) | 29'-4" | 27'-9'(1) | 22'-2"(1) | 26'-10" | 25'-7'(1) | 21'-6 ${ }^{\prime \prime}$ (1) | 28'-5' | 27'-0'11) | 22'-2'(1) |
|  | 560 | 30'-2'' | 28'-9' | 25'-2'11) | 31'-11" | 30'-5'(1) | 27'-5"(1) | 29'-5" | 28'-0" | 25'-2'11) | 31'-2' | 29'-7" | 27'-5"(1) |
| 22" | 560D | $32^{\prime}-2{ }^{\prime \prime}$ | $30^{\prime}-8{ }^{\prime \prime}$ | 28'-10'1 | $34^{\prime}-7{ }^{\prime \prime}$ | 32'-5" | $30^{\prime}-6^{\prime \prime}$ | 31'-5' | 29'-10'1 | 28'-0'1 | $33^{\prime}-5^{\prime \prime}$ | $31^{\prime}-6{ }^{\prime \prime}$ | 29'-8' |
| 24" | 560D | 34'-6' | $32 '-4$ ' | $30^{\prime}-6{ }^{\prime \prime}$ | 37'-2' | 34'-10' | 32'-3' | $33^{\prime}-5{ }^{\prime \prime}$ | 31'-6' | 29'-7' | 35'-11' | $33^{\prime}-7{ }^{\prime \prime}$ | $31^{\prime}-3^{\prime \prime}$ |
| 40 PSF Live Load / 30 PSF Dead Load |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 18" | 360 | 26'-0'(1) | 21-9'1(1) | 17'-4'(1) | $26^{\prime}-11^{1 /(1)}$ | 22'-5"(1) | 17'-11'(1) | 25'-2'11) | 21'-9'1(1) | 17'-4'(1) | 26'-7'(1) | 22'-5"(1) | 17'-11'(1) |
|  | 560 | 28'-3' | 25'-5 ${ }^{\prime \prime}(1)$ | $20^{\prime}-4^{\prime \prime}(1)$ | 29'-11'(1) | $27^{\prime}-8^{\prime \prime}(1)$ | $22^{\prime}-1^{\prime \prime}(1)$ | 27'-7' | 25'-5'(1) | $20^{\prime}-4^{\prime \prime}(1)$ | 29'-2'11) | $27^{-}-8^{\prime \prime}(1)$ | $22^{\prime}-1{ }^{\prime \prime}(1)$ |
| 20" | 360 | 26'-1'11) | 21-9'1(1) | $17^{\prime}-4^{\prime \prime}(1)$ | $26^{\prime}-11^{1 /(1)}$ | 22'-5"(1) | 17'-11'(1) | 26'-1'(1) | 21'-9'1(1) | $17^{\prime}-4^{\prime \prime}(1)$ | $26^{\prime}-11^{\prime \prime}(1)$ | 22'-5"(1) | 17'-11'(1) |
|  | 560 | $30^{\prime}-2^{\prime \prime}(1)$ | 25'-5"(1) | 20'-4'11) | $31^{\prime}-11^{\prime \prime}(1)$ | $27^{\prime}-8^{\prime \prime}(1)$ | 22'-1'(1) | 29'-5'11) | 25'-5'(1) | 20'-4'(1) | $31^{\prime}-2^{\prime \prime}(1)$ | $27^{-}-8^{\prime \prime}(1)$ | 22'-1'(1) |
| 22" | 560D | 32'-2" | $30^{\prime}-8^{\prime \prime}$ | 28'-10'1 | 34'-7' | $32^{\prime}-5^{\prime \prime}$ | 29'-7" | $31^{\prime \prime}-5^{\prime \prime}$ | 29'-10'1 | 28'-0'1 | 33'-5' | $31^{\prime}-6^{\prime \prime}$ | 29'-7' |
| 24" | 560D | 34'-6' | 32'-4' | $30^{\prime}-6{ }^{\prime \prime}$ | 37'-2' | 34'-10" | $31^{\prime}-6{ }^{\prime \prime}$ | $33^{\prime}-5{ }^{\prime \prime}$ | 31'-6" | 29'-7" | 35'-11' | $33^{\prime}-7{ }^{\prime \prime}$ | $31^{\prime}-3{ }^{\prime \prime}$ |

(1) Web stiffeners are required at intermediate supports of continuous-span joists when the intermediate bearing length is less than $51 / 4$ " and the span on either side of the intermediate bearing is greater than the following spans:

| TJ® | 40 PSF Live Load / 15 PSF Dead Load |  |  | 40 PSF Live Load / 30 PSF Dead Load |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 16" o.c. | 19.2" o.c. | 24" o.c. | 16" o.c. | 19.2" o.c. | 24" o.c. |
| 360 | Not Required | 24'-6' | 19'-7" | 23'-9" | 19'-9" | 15'-10" |
| 560 |  | 29'-11" | 23'-11" | 29'-0" | 24'-2" | 19'-3" |

- Bold italic spans indicate floors that would meet National Building Code of Canada (NBCC) vibration criteria but would be considered by $35 \%$ of the population to have marginal or unacceptable performance.


## How to Use These Tables

1. Determine the the subflooring thickness and applicable live and dead loads.
2. Determine whether the ceiling will be directly applied and what the span condition is (simple or continuous).
3. Select on-centre spacing.
4. Scan down the column until you meet or exceed the span of your application.
5. Select $T J \|^{®}$ joist and depth.

## General Notes

- Tables are based on:
- Clear distance between supports.
- 18" and 20" TJI ${ }^{\circledR}$ joists: Minimum bearing length of $13 / 4^{\prime \prime}$ end (no web stiffeners) and $31 / 2^{\prime \prime}$ intermediate.
- 22" and 24" TJI® joists: Minimum bearing length of $13 / 4^{\prime \prime}$ end and $31 / 2^{\prime \prime}$ intermediate; web stiffeners required at all bearings.
- Limit States Design per CSA 086.
- Uniform loads.
- Single layer of appropriate span-rated OSB.
- NBCC vibration criteria as ratified by Canadian Construction Materials Centre (CCMC).
- Long term deflection under dead load, which includes the effect of creep, has not been considered.
- For continuous spans, ratio of short span to long span should be 0.4 or greater to prevent uplift.
- Spans generated from Weyerhaeuser software may exceed the spans shown in these tables because software reflects actual design conditions.
- For multi-family applications and other loading conditions not shown, refer to Weyerhaeuser software.

Maximum Horizontal Clear Spans- Roof (slopes of 3:12 or less)

| O.C. Spacing | Depth | TJ® | Unfactored Snow Load (LL) and Dead Load (DL) in PSF |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 25LL + 15DL | 30LL + 15DL | 40LL + 15DL | 50LL + 15DL |
| 16" | 18" | 360 | 35'-3" | 33'-1' | 29'-6" | 24'-9" |
|  |  | 560 | 40'-5" | 37'-11" | $34^{\prime}-4{ }^{\prime \prime}$ | 30'-2" |
|  | 20" | 360 | 38'-2" | 35'-10" | 29'-6" | 24'-9" |
|  |  | 560 | 43'-9" | $41^{\prime}-1{ }^{\prime \prime}$ | $35 '-11{ }^{\prime \prime}$ | 30'-2" |
|  | 22" | 560D | 47'-4' | 44'-5' | $40^{\prime}-2{ }^{\prime \prime}$ | 37'-2' |
|  | 24" | 560D | $50^{\prime}-6{ }^{\prime \prime}$ | 47'-5' | 42'-11" | $39^{\prime}-8{ }^{\prime \prime}$ |
| 19.2" | 18" | 360 | 33'-1" | 30'-4" | 24'-6" | 20'-7" |
|  |  | 560 | 37'-11" | $35^{\prime}-7{ }^{\prime \prime}$ | 29'-11" | 25'-1" |
|  | 20" | 360 | 34'-5" | 30'-4" | 24'-6" | 20'-7" |
|  |  | 560 | 41'-1' | 37'-0" | 29'-11" | 25'-1" |
|  | 22" | 560D | 44'-5' | $41^{\prime}-8^{\prime \prime}$ | 37'-8" | 34'-10'1 |
|  | 24" | 560D | 47'-5' | 44'-6' | $40^{\prime}-3{ }^{\prime \prime}$ | 37'-3' |
| $24 "$ | 18" | 360 | 27'-6" | 24'-3" | 19'-7" | $16^{\prime}-5{ }^{\prime \prime}$ |
|  |  | 560 | $33^{\prime}-6{ }^{\prime \prime}$ | 29'-7" | 23'-11" | 20'-1" |
|  | 20" | 360 | $27^{\prime}-6{ }^{\prime \prime}$ | 24'-3" | 19'-7" | 16'-5" |
|  |  | 560 | $33^{\prime}-6{ }^{\prime \prime}$ | 29'-7" | 23'-11" | 20'-1' |
|  | 22" | 560D | 41'-1' | 38'-7' | $34^{\prime}-10^{\prime \prime}$ | 30'-10" |
|  | 24" | 560D | 43'-11' | $41^{\prime}-2^{\prime \prime}$ | $37^{\prime}-3^{\prime \prime}$ | 32'-9'1 |

## How to Use This Table

1. Determine appropriate unfactored snow and dead load.
2. Scan down the column until you find a span that meets or exceeds the span of your application.
3. Select $T J{ }^{®}$ joist and on-centre spacing.

## General Notes

- Table is based on:
$-18{ }^{\prime \prime}$ and 20 " TJI ${ }^{®}$ joists: Minimum bearing length of $13 / 4$ " end and $31 / 2$ " intermediate (no web stiffeners).
-22 " and $24^{\prime \prime} \mathrm{TJ}{ }^{®}$ joists: Minimum bearing length of $13 / 4^{\prime \prime}$ end and $31 / 2^{\prime \prime}$ intermediate; web stiffeners required at all bearings.
- Uniform loads.
- More restrictive of simple or continuous span.
- Roof slopes of $1 / 4: 12$ minimum, 3:12 maximum.
- Unfactored total load joist deflection limited to L/180.
- Unfactored live load joist deflection limited to L/360.
- For continuous spans, ratio of short span to long span should be 0.4 or greater to prevent uplift.
- A support beam or wall at the high end is required. Ridge board applications do not provide adequate support.
- For flat roofs or other loading conditions not shown, refer to Weyerhaeuser software.


## R00F LOAD TABLE

Roof-Factored Resistance, Standard Term (PLF) (slopes of 3:12 or less)

| Depth | TJ® | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance | Unfactored Deflection Resistance |  | Factored Strength Resistance |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Live } \\ & \text { Load } \\ & \text { L/360 } \end{aligned}$ | Total Load L/180 | Total Load | Live Load L/360 | Total Load L/180 | Total Load | $\begin{aligned} & \text { Live } \\ & \text { Load } \\ & \text { L/360 } \end{aligned}$ | Total Load L/180 | Total Load | $\begin{aligned} & \text { Live } \\ & \text { Load } \end{aligned}$ $\mathrm{L} / 360$ | Total Load L/180 | Total Load | Live Load L/360 | Total <br> Load <br> L/180 | Total Load |
|  |  | Roof Joist Horizontal Clear Span |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 12' |  |  | $14^{\prime}$ |  |  | $16^{\prime}$ |  |  | 18' |  |  | $20^{\prime}$ |  |  |
| 18" | 360 | * | * | 255 | * | * | 219 | * | * | 192 | * | * | 171 | * | * | 154 |
|  | 560 | * | * | 311 | * | * | 267 | * | * | 234 | * | * | 208 | * | * | 188 |
| 20" | 360 | * | * | 255 | * | * | 219 | * | * | 192 | * | * | 171 | * | * | 154 |
|  | 560 | * | * | 311 | * | * | 267 | * | * | 234 | * | * | 208 | * | * | 188 |
| 22" | 560D | * | * | 477 | * | * | 410 | * | * | 359 | * | * | 319 | * | * | 288 |
| 24" | 560D | * | * | 508 | * | * | 436 | * | * | 382 | * | * | 340 | * | * | 306 |
|  |  | $22^{\prime}$ |  |  | $24^{\prime}$ |  |  | $26^{1}$ |  |  | $28^{\prime}$ |  |  | $30^{\prime}$ |  |  |
| 18" | 360 | * | * | 140 | * | * | 128 | 81 | * | 118 | 66 | * | 110 | 54 | * | 103 |
|  | 560 | * | * | 171 | * | * | 156 | * | * | 144 | * | * | 134 | 80 | * | 125 |
| 20" | 360 | * | * | 140 | * | * | 128 | * | * | 118 | * | * | 110 | 68 | * | 103 |
|  | 560 | * | * | 171 | * | * | 156 | * | * | 144 | * | * | 134 | * | * | 125 |
| 22" | 560D | * | * | 262 | * | * | 240 | * | * | 221 | * | * | 206 | 124 | * | 192 |
| 24" | 560D | * | * | 278 | * | * | 255 | * | * | 236 | * | * | 219 | * | * | 204 |

* Indicates value does not control.


## How to Use This Table

1. Calculate actual factored total load and unfactored snow and total load on the joist in pounds per linear foot (plf).
2. Select appropriate Roof Joist Horizontal Clear Span. For slopes greater than 2:12 (up to a maximum of $3: 12$ ), approximate the increased dead load by multiplying the joist horizontal clear span by the Slope Factor on page 33.
3. Scan down the columns to find a $\mathrm{TJI}^{\circledR}$ joist that meets or exceeds the actual unfactored snow and total loads, and the factored total load. All three columns must be checked.

## General Notes

- Table is based on:
- $18^{\prime \prime}$ and $20^{\prime \prime} \mathrm{TJ}{ }^{\circledR}$ joists: Minimum bearing length of $13 / 4^{\prime \prime}$ end (no web stiffeners) and $31 / 2^{\prime \prime}$ intermediate.
- 22" and 24" TJI ${ }^{\circledR}$ joists: Minimum bearing length of $13 / 4^{\prime \prime}$ end and $31 / 2^{\prime \prime}$ intermediate; web stiffeners required at all bearings.
- Uniform loads.
- More restrictive of simple or continuous span.
- Roof slopes of $1 / 4: 12$ minimum, 3:12 maximum.
- No composite action provided by sheathing.



## These Conditions Are NOT Permitted:



DO NOT use sawn lumber for rim board or blocking as it may shrink after installation. Use only engineered lumber


DO NOT bevel cut joist beyond inside face of wall.


DO NOT install hanger overhanging face of plate or beam. Flush bearing plate with inside face of wall or beam.

Cantilevers Less than 5" (Brick Ledge) See Section A of cantilever table


Cantilevers 5" to 24"

## See Section B of cantilever table



## Cantilever Reinforcement

| Depth | TJ® | $\begin{aligned} & \text { Roof } \\ & \text { Truss } \\ & \text { Span } \end{aligned}$ | Section A: Cantilevers less than 5" (Brick Ledge) |  |  |  |  |  |  |  |  | Section B: Cantilevers 5" to 24" |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 35 PSF |  |  | 45 PSF |  |  | 55 PSF |  |  | 35 PSF |  |  | 45 PSF |  |  | 55 PSF |  |  |
|  |  |  | On-Centre Joist Spacing |  |  |  |  |  |  |  |  | On-Centre Joist Spacing |  |  |  |  |  |  |  |  |
|  |  |  | 16" | 19.2" | 24" | $16^{\prime \prime}$ | 19.2" | 24" | $16^{\prime \prime}$ | 19.2" | 24" | $16^{\prime \prime}$ | 19.2" | $24 "$ | $16{ }^{\prime \prime}$ | 19.2" | $24{ }^{\prime \prime}$ | $16^{\prime \prime}$ | 19.2" | 24" |
| $\begin{aligned} & 18 " \\ & \text { or } \\ & 200^{\prime \prime} \end{aligned}$ | 360 | 22' |  |  |  |  |  | X |  | X | X |  |  |  |  |  |  |  |  |  |
|  |  | $24^{\prime}$ |  |  | X |  |  | X |  | X | X |  |  |  |  |  |  |  |  |  |
|  |  | $26^{\prime}$ |  |  | X |  | X | X |  | X | X |  |  |  |  |  |  |  |  | E1W |
|  |  | $28^{\prime}$ |  |  | X |  | X | X | X | X | X |  |  |  |  |  |  |  |  | E1W |
|  |  | $30^{\prime}$ |  |  | X |  | X | X | X | X | X |  |  |  |  |  |  |  |  | X |
|  |  | $32^{\prime}$ |  | X | X |  | X | X | X | X | X |  |  |  |  |  | E1W |  |  | X |
|  |  | $34^{\prime}$ |  | X | X | X | X | X | X | X | X |  |  |  |  |  | E1W |  |  | X |
|  |  | $36^{\prime}$ |  | X | X | X | X | X | X | X | X |  |  |  |  |  | E1W |  | E1W | X |
|  |  | 38' |  | X | X | X | X | X | X | X | X |  |  |  |  |  | X |  | E1W | X |
|  |  | $40^{\prime}$ | X | X | X | X | X | X | X | X | X |  |  | E1W |  |  | X |  | E1W | X |
| $\begin{aligned} & 18 " \\ & \text { or } \\ & 20 " \end{aligned}$ | 560 | $22^{\prime}$ |  |  |  |  |  |  |  |  | X |  |  |  |  |  |  |  |  |  |
|  |  | $24^{\prime}$ |  |  |  |  |  | X |  |  | X |  |  |  |  |  |  |  |  |  |
|  |  | $26^{\prime}$ |  |  |  |  |  | X |  | X | X |  |  |  |  |  |  |  |  |  |
|  |  | $28^{\prime}$ |  |  |  |  |  | X |  | X | X |  |  |  |  |  |  |  |  |  |
|  |  | $30^{\prime}$ |  |  | X |  |  | X |  | X | X |  |  |  |  |  |  |  |  |  |
|  |  | 32' |  |  | X |  | $x$ | X | $x$ | X | X |  |  |  |  |  |  |  |  |  |
|  |  | $34^{\prime}$ |  |  | X |  | X | X | X | X | X |  |  |  |  |  |  |  |  | E1W |
|  |  | $36^{\prime}$ |  |  | X |  | X | X | X | X | X |  |  |  |  |  |  |  |  | E1W |
|  |  | $38^{\prime}$ |  | X | X | X | X | X | X | X | X |  |  |  |  |  |  |  |  | E1W |
|  |  | $40^{\prime}$ |  | X | X | X | X | X | X | X | X |  |  |  |  |  |  |  |  | X |
| $\begin{aligned} & 22 " \\ & \text { or } \\ & 244^{\prime \prime} \end{aligned}$ | 5600 | $22^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $24^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $26^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $28^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $30^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $32^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | , | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $34^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | $x$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $36^{\prime}$ | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | X | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $38^{\prime}$ | E1W | E1W | E1W | E1W | E1W | X | E1W | E1W | x | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |
|  |  | $40^{\prime}$ | E1W | E1W | E1W | E1W | E1W | X | E1W | E1W | X | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W | E1W |

## How to Use This Table

1. Identify $\mathrm{TJ}{ }^{\circledR}$ joist and depth.
2. Locate the Roof Truss Span (horizontal) that meets or exceeds your condition.
3. Identify the cantilever condition (less than 5 " or 5 " to 24 ") and locate the Unfactored Roof Total Load and On-Centre Joist Spacing for your application.
4. Scan down to find the appropriate cantilever detail and refer to drawing on page 20:

- Blank cells indicate no reinforcement is required.
- X indicates cantilever will not work. Use ForteWEBTM or Javelin ${ }^{\circledR}$ software, or reduce spacing of joists and recheck table.


## General Notes

- Table is based on:
- 15 psf unfactored roof dead load on a horizontal projection.
- 80 plf unfactored exterior wall load with 3'-0" maximum width window or door openings. For larger openings, or multiple $3^{\prime}-0^{\prime \prime}$ width openings spaced less than $6^{\prime}-0$ " on-centre, additional joists beneath the opening's trimmers may be required.
- 40/15 psf floor load.
- More restrictive of simple or continuous span.
- Roof truss with 24" soffits.
- Designed for $2 \times 4$ and $2 \times 6$ plate widths.
- For conditions beyond the scope of this table, including cantilevers longer than 24 ", use ForteWEB ${ }^{\text {TM }}$ or Javelin ${ }^{\circledR}$ software.


## See page 20 for cantilever details.



Single Joist, Top Mount


Single Joist, Face Mount


Face Mount Skewed 45 Joist Hanger


Double Joist, Top Mount


Double Joist, Face Mount

Variable Slope Seat Joist Hanger


Variable Slope Seat Connector

| Depth | TJI® | Single Joist-Top Mount |  |  |  | Single Joist-Face Mount |  |  |  | Face Mount Skewed 45 Joist Hanger |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |  |  | Header | Joist |
| 18" | 360 | MIT3518 | 1,995 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2 \mathrm{\prime} \mathrm{\prime}$ | MIU2.37/18 | 1,995 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SUR/L2.37/14 | 2,260 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{1¹/2"}$ |
|  | 560 | MIT418 | 2,305 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11⁄2"}$ | MIU3.56/18 | 2,305 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SUR/L414 | 2,360 | 16d | 16d |
| 20" | 360 | MIT3520 | 1,995 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | MIU2.37/20 | 1,995 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SUR/L2.37/14 | 2,260 | 16d | 10d x 11/2" |
|  | 560 | MIT420 | 2,305 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | MIU3.56/20 | 2,305 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SUR/L414 | 2,360 | 16d | 16 d |
| 22" | 560D | HIT422 | 2,705 | 16d | $10 \mathrm{~d} \mathrm{x} \mathrm{11⁄2"}$ | MIU3.56/20 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SUR/L4144) | 2,895 | 16d | 16d |
| 24" | 560D | HIT424 | 2,705 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | MIU3.56/20 | 3,485 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SUR/L41444) | 2,895 | 16d | 16d |


| Depth | TJ® | Double Joist-Top Mount |  |  |  | Double Joist-Face Mount |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |
| 18" | 360 | BA4.75/18 | 4,370 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | MIU4.75/18 | 3485 | 16d | 10d x $11 / 2{ }^{1}$ |
|  | 560 | HB7.12/18 | 5,450 | 16d | 16 d | HU414-2 | 4615 | 16d | 16 d |
| 20" | 360 | BA4.75/20 | 4,370 | 16d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | MIU4.75/20 | 3485 | 16d | 10d x $11 / 2^{\prime \prime}$ |
|  | 560 | HB7.12/20 | 5,450 | 16d | 16d | HU414-2 | 4615 | 16d | 16d |
| 22" | 560D | HB7.12/22 | 5,945 | 16d | 16d | HU414-2 | 4690 | 16d | 16d |
| 24" | 560D | HB7.12/24 | 5,945 | 16d | 16d | HU414-2 ${ }^{(4)}$ | 4690 | 16d | 16d |

Hanger information in this section was provided by Simpson Strong-Tie ${ }^{\circledR}$. For additional information, please refer to their literature.

| Depth | TJ® | Variable Slope Seat Joist Hanger ${ }^{(2)}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) |  | Nailing |  |
|  |  |  | Sloped Only | $\begin{aligned} & \text { Sloped } \\ & \text { and } \\ & \text { Skewed } \end{aligned}$ | Header | Joist |
| 18"-20" | 360 | LSSR2.372 | 1,560 | 1,200 | 10d | 10d x 1¹/2" |
|  | 560 | LSSR410Z | 2,045 | 1,835 | 16d | 16d |
| 22"-24" | 560D | LSSR410Z | 2,395 | 1,835 | 16d | 16d |


| Depth | TJI® | Variable Slope Seat Connector ${ }^{(1)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |
| 18"-20" | 360 | VPA35 | 1,805 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 560 | VPA4 | 1,855 | 10d | $10 \mathrm{~d} \times 11 / 2{ }^{\prime \prime}$ |
| 22"-24" | 560D | VPA4 | 1,855 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |

## General Notes

Bold italic hangers require web stiffeners.
Factored resistances will vary with different nailing criteria or other support conditions; contact your Weyerhaeuser representative for assistance.

- Hanger factored resistances shown are either joist bearing or hanger factored resistance-whichever is less. Joist end reaction must be checked to ensure it does not exceed the factored resistance shown in the tables.
- All factored resistances are for downward loads, standard term.
- Fill all round, dimple, and positive-angle nail holes.
- Use sloped seat hangers and beveled web stiffeners when TJI® joist slope exceeds $1 / 4: 12$. Maximum slope for $18{ }^{\prime \prime}-24^{\prime \prime}$ TJI® joists is 3:12.
- Leave $1 / 16^{\prime \prime}$ clearance ( $1 / 88^{\prime \prime}$ maximum) between the end of the supported joist and the header or hanger.
- Nails: $16 \mathrm{~d}=0.162^{\prime \prime} \times 31 / 2^{\prime \prime}, 10 \mathrm{~d}=0.148^{\prime \prime} \times 3^{\prime \prime}$, and $10 \mathrm{~d} \times 1 / 22^{\prime \prime}=0.148^{\prime \prime} \times 11 / 2^{\prime \prime}$.


Single Joist, Top Mount


Single Joist, Face Mount


Face Mount Skewed $45^{\circ}$ Joist Hanger


Double Joist, Top Mount


Double Joist, Face Mount



Variable Slope Seat Connector

| Joist |  | Single Joist-Top Mount |  |  |  | Single Joist-Face Mount |  |  |  | Face Mount Skewed $45^{\circ}$ Joist Hanger |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | TJI® | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  |
| D |  |  |  | Header | Joist |  |  | Header | Joist |  |  | Header | Joist |
| 18" | 360 | TFI3518 | 1,995 | 16d | $10 \mathrm{~d} \times 1$ 1⁄2" | IHF2318 | 1,995 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | SKH2324L/R | 1,755 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11⁄2"}$ |
| 10 | 560 | TFI418 | 2,305 | 16d | $10 \mathrm{~d} \times 11 / 2 \mathrm{~L}$ | IHF3518 | 2,305 | 10d | $10 \mathrm{~d} \times 1$ 1/2" | SKH414L/R ${ }^{(3)}$ | 2,305 | 16d | 16 d |
| 20" | 360 | TFI3520 | 1,995 | 16d | $10 \mathrm{~d} \times 11 / 21$ | IHF2318 | 1,995 | 10d | $10 \mathrm{~d} \times 1$ 1⁄2" | SKH2324L/R ${ }^{(4)}$ | 1,755 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ |
| 20 | 560 | TFI420 | 2,305 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | IHF3518 | 2,305 | 10d | $10 \mathrm{~d} \times 11 / 2 \mathrm{\prime} \mathrm{\prime}$ | SKH414L/R ${ }^{(3)}$ | 2,305 | 16d | 16d |
| 22" | 560D | TFI422 | 3,680 | 16d | $10 \mathrm{~d} \times 11 / 2{ }^{\text {" }}$ | IHF3518 | 3,310 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ | SKH414L/R ${ }^{(3)(4)}$ | 3,680 | 16d | 16d |
| 24" | 560D | TFI424 | 3,680 | 16d | $10 \mathrm{~d} \times 11 / 2{ }^{\text {" }}$ | IHF3518 | 3,310 | 10d | $10 \mathrm{~d} \times 11 / 2^{\prime \prime}$ | SKH414L/R ${ }^{(3) / 4)}$ | 3,680 | 16d | 16d |

(1) Miter cut is required at end of joists.

| Joist |  | Double Joist-Top Mount |  |  |  | Double Joist-Face Mount |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Depth | TJ® | Hanger | Fac. Res. (lbs) | Nailing |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |  |  | Header | Joist |
| 18" | 360 | TH023180-2 | 4,375 | 16d | 10d | THF23160-2 | 3,990 | 10d | 10d |
|  | 560 | BPH7118 | 4,305 | 16d | 10d | HD7160 | 4,615 | 16d | 10d |
| 20" | 360 | TH023200-2 | 4,375 | 16d | 10d | THF23160-2 | 3,990 | 10d | 10d |
|  | 560 | BPH7120 | 4,305 | 16d | 10d | HD7160 | 4,615 | 16d | 10d |
| 22" | 560D | BPH7122 | 4,305 | 16d | 10d | HD7160 | 4,710 | 16d | 10d |
| 24 | 560D | BPH7124 | 4,305 | 16d | 10d | HD7160 | 4,710 | 16d | 10d |

Hanger information in this section was provided by USP Structural Connectors ${ }^{\circledR}$. For additional information, please refer to their literature.

| Depth | TJI® | Variable Slope Seat Joist Hanger ${ }^{(2)}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) |  | Nailing |  |
|  |  |  | Sloped Only | $\begin{gathered} \text { Sloped } \\ \text { and } \\ \text { Skewed } \end{gathered}$ | Header | Joist |
| 18"-20" | 360 | LSSH23 | 1,990 | 1,990 | 10d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
|  | 560 | LSSH35 | 2,515 | 2,390 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |
| 22"-24" | 560D | LSSH35 | 3,890 | 2,390 | 16d | $10 \mathrm{dx} \mathrm{1} 1 / 2^{\prime \prime}$ |


| Depth | TJI® | Variable Slope Seat Connector ${ }^{(5)}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Hanger | Fac. Res. (lbs) | Nailing |  |
|  |  |  |  | Header | Joist |
| 18"-20" | 360 | TMP23 | 2,175 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
|  | 560 | TMP4 | 2,175 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |
| 22"-24" | 560D | TMP4 | 2,175 | 10d | $10 \mathrm{~d} \mathrm{x} \mathrm{11/2"}$ |

## Support Requirements

- Support material assumed to be Trus Joist® engineered lumber or sawn lumber (Douglas fir, southern pine, or spruce-pine-fir species).
- Minimum support width for single- and double-joist top mount hangers is 3 ".
- Minimum support width for face mount hangers with 10 d and 16 d nails (clinched) is $11 / 2$ and $13 / 4$ ", respectively.

Also see General Notes on page 22.

Table footnotes for pages 22 and 23:
(1) For joists 18 " and deeper, use VPA for 3:12 slopes only.
(2) For joists $18^{\prime \prime}$ and deeper, use only with slopes up to $3: 12$ and skews up to $45^{\circ}$. Additional lateral restraint required for $18^{\prime \prime}$ and $20^{\prime \prime}$ joists.
(3) Miter cut required at end of joist.
(4) Additional lateral restraint required.
(5) For joist depths 18 " and deeper, use only on slopes of 1:12 to 3:12.


Table A—End Support (Minimum distance from edge of hole to inside face of nearest end support)

| Depth | TJ ${ }^{\text {® }}$ | Round Hole Size |  |  |  |  |  |  |  |  |  | $\square$ Square or Rectangular Hole Size |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 4" | 5" | 6" | 6112" | 7" | 8" | 101 | 12" | 143/4" | 163/4" | 4" | 5" | $6{ }^{\prime \prime}$ | 61/2" | 7" | 8" | 101 | 12" | 143/4" | 163/4" |
| 18" | 360 | 1'-0" | 1'-0" | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | 2'-0" | 4'-0" | 5'-6" | 9'-6" |  | 1'-0" | $1^{\prime}-6{ }^{\prime \prime}$ | 3'-0" | 4'-0" | 4'-6" | $6^{\prime}-0{ }^{\prime \prime}$ | 10'-0" | 11'-0" | 13'-6" |  |
|  | 560 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | 4'-6" | 7'-0" | 10'-6" |  | 2'-0" | 3'-6" | 5'-0" | 5'-6" | 6'-6" | 8'-0" | 11'-0" | 12'-0" | 14'-0" |  |
| 20" | 360 | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | 1'-0" | 2'-0" | 4'-0" | 7'-0" | $10^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | $1^{1}-0{ }^{\prime \prime}$ | 1'-6" | 2'-0" | $3^{1}-0{ }^{\prime \prime}$ | 4'-6" | $8^{\prime}-0{ }^{\prime \prime}$ | 11'-6" | 13'-6" | 15'-6" |
|  | 560 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 2'-0" | 4'-6" | 8'-6" | 11'-0' | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 3'-6" | $4^{\prime}-6{ }^{\prime \prime}$ | 5'-0" | 7'-0" | 10'-6" | 13'-0" | 14'-6" | 15'-6" |
| 22" | 560D | 1'-0" | $1^{1}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-0{ }^{\prime \prime}$ | 1'-6" | $3^{1}-6{ }^{\prime \prime}$ | 5'-0' | 7'-0'1 | 9'-6" | $1^{1}-0^{\prime \prime}$ | 2'-6" | 3'-6" | 4'-6" | 5'-0'1 | $6^{\prime}-6{ }^{\prime \prime}$ | 14'-6' | $15^{\prime}-0{ }^{\prime \prime}$ | $16^{\prime}-0^{\prime \prime}$ | 16'-6' |
| 24 " | 560D | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{1}-6{ }^{\prime \prime}$ | 2'-0' | $3^{1}-6{ }^{\prime \prime}$ | 5'-0'1 | 7'-0'1 | 8'-6'1 | 1'-6" | 2'-6" | $4^{\prime}-0^{\prime \prime}$ | 4'-6" | 5'-0'1 | $6^{\prime}-6^{\prime \prime}$ | 9'-6" | 15'-0' | $16^{\prime}-0^{\prime \prime}$ | 16'-6' |

## Table B—Intermediate or Cantilever Support

(Minimum distance from edge of hole to inside face of nearest intermediate or cantilever support)

| Depth | TJI® | Round Hole Size |  |  |  |  |  |  |  |  |  | $\square$ Square or Rectangular Hole Size |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 4" | 5" | 6" | 61/2" | 7" | 8" | 10" | 12" | 143/4" | 163/4" | 4" | 5" | $6{ }^{\prime \prime}$ | 61/2" | 7" | 8" | $10^{\prime \prime}$ | 12" | 143/4" | 163/4" |
| 18" | 360 | 1'-0" | 1'-0" | 1'-0" | $1^{\prime \prime}-0{ }^{\prime \prime}$ | 1'-6" | 3'-0" | $6^{\prime}-0{ }^{\prime \prime}$ | 9'-0" | 14'-6" |  | 1'-0" | $1^{\prime}-6{ }^{\prime \prime}$ | 4'-0" | 5'-6" | 6'-6" | 9'-0" | 14'-6" | 16'-6" | 19'-0" |  |
|  | 560 | 1'-0" | 1'-0" | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $2^{\prime}-0{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | 10'-0' | $15^{\prime}-6{ }^{\prime \prime}$ |  | $1^{\prime}$-0" | $3^{\prime}-6{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | 7'-6" | 8'-6" | 11'-6" | $16^{\prime}-6{ }^{\prime \prime}$ | 18'-0" | 19'-6" |  |
| 20" | 360 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-0{ }^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | $11^{\prime}-0{ }^{\prime \prime}$ | 15'-0" | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-6" | 2'-6" | 4'-0" | 7'-0" | 12'-6" | 16'-6" | 19'-0" | 20'-6" |
|  | 560 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 5'-6" | $11^{\prime}-6{ }^{\prime \prime}$ | 15'-6" | $1^{\prime}$-0" | $1^{\prime}-0{ }^{\prime \prime}$ | $3^{\prime}-0^{\prime \prime}$ | 4'-6" | $6^{\prime}-0{ }^{\prime \prime}$ | 8'-6" | 14'-0" | 17'-6" | 19'-0" | 20'-6" |
| 22" | 560D | 1'-0' | $1^{\prime}-6{ }^{\prime \prime}$ | 2'-6" | 3'-0' | 3'-6" | 4'-6' | $6^{1}-6{ }^{\prime \prime}$ | 8'-0' | 11'-0' | 14'-6' | 3'-6" | 5'-0" | $6^{\prime}-6{ }^{\prime \prime}$ | 7'-6" | 8'-6" | 10'-0' | 19'-0' | 20'-0' | 21'-0' | 21'-6" |
| 24" | 560D | 2'-6' | $3^{\prime}-0^{\prime \prime}$ | $4^{\prime}-0^{\prime \prime}$ | 4'-6' | $5^{\prime}-0^{\prime \prime}$ | $5^{\prime}-6{ }^{\prime \prime}$ | $7^{\prime}-0{ }^{\prime \prime}$ | 8'-6' | $11^{\prime}-0^{\prime \prime}$ | 13'-6'\| | $5^{\prime}-0^{\prime \prime}$ | $6^{\prime}-0{ }^{\prime \prime}$ | 7'-6" | $8^{\prime}-0{ }^{\prime \prime}$ | $9^{\prime}-0{ }^{\prime \prime}$ | $10^{\prime}-6{ }^{\prime \prime}$ | $14^{\prime}-0^{\prime \prime}$ | 20'-0' | $21^{\prime}-0^{\prime \prime}$ | 21'-6' |

- Rectangular holes based on measurement of longest side.


## How to Use These Tables

1. Using Table A, Table B, or both if required, determine the hole shape/size and select the $\mathrm{TJ}{ }^{\circledR}$ joist and depth.
2. Scan horizontally until you intersect the correct hole size column.
3. Measurement shown is minimum distance from edge of hole to support.
4. Maintain the required minimum distance from the end and the intermediate or cantilever support.

## General Notes

- Holes may be located vertically anywhere within the web. Leave $1 / 8^{\prime \prime}$ of web (minimum) at top and bottom of hole.
- Knockouts are located in web at approximately 12" on-centre; they do not affect hole placement and may be located in the hatched zone.
- For simple span ( 5 ' minimum) uniformly loaded joists meeting the requirements of this guide, one maximum size round hole may be located at the centre of the joist span provided that no other holes occur in the joist.
- Distances are based on the maximum uniform loads shown in this guide. For other load conditions or hole configurations, use ForteWEBTM software or contact your Weyerhaeuser representative.


## This section contains framing details and design information applicable to all joist depths shown in this guide.



TJI® Joist Nailing Requirements at Bearing

## TJI® Joist to Bearing Plate



Squash Blocks to TJI® Joist (Load bearing wall above)


Also see detail B2 on page 27.

Locate rim board joint between joists


A1 A1 Attach blocking per fastening instructions in Detail A3.


## Exterior Deck Attachment



Shimmed Deck Attachment


Ledger Fastener ${ }^{(1)}$ Factored Resistances

| Rim Board Material | Factored Resistance Load ${ }^{(2)}$ ( $\mathrm{lbs} / \mathrm{bolt}$ ) |  |  |
| :---: | :---: | :---: | :---: |
|  | 1/2" Lag Bolt | 1⁄2" Through Bolt | $1 / 22^{1}$ Through Bolt with Air Space |
| 11/8" TJ® Rim Board ${ }^{(3)}$ | 695 | 1,005 | 890(4) |
| 11/4" TimberStrand ${ }^{\text {® }}$ LSL | 885 | 1,050 |  |
| 11⁄2" TimberStrand ${ }^{\text {® }}$ LSL | 980 | 1,050 |  |

(1) Corrosion-resistant fasteners required in wet-service applications
(2) Factored resistance determined in accordance with ASTM 7672.
(3) $1^{1} / 8^{\prime \prime} \mathrm{TJ}{ }^{\circledR}$ Rim Board is allowed with joist depths $\leq 16^{\prime \prime}$ only.
(4) Maximum $1 / 2$ " shimmed air space.

## General Notes

- Maintain 2" distance (minimum) from edge of ledger to fastener. Stagger bolts.
- Local building codes may require through bolts with washers.
- Lateral restraining connections may be required.
- See Weyerhaeuser's Rim Board Specifier's Guide, TJ-8500, for more information.


## Vertical Load Transfer at Bearing

| Rim or Blocking Material | Uniform Load (PLF) |  |  |  |  |  | $\begin{gathered} \text { Concentrated } \\ \text { Load (lbs) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Depth |  |  |  |  |  |  |
|  |  | 16" | 18" | 20" | 22" | 24" | All Depths |
| TJI® rim joist | 3,060 |  | 2,250 |  | 2,475 ${ }^{(1)}$ |  | - |
| 11/8" TJ ${ }^{\text {® }}$ Rim Board | $7,045{ }^{(2)} \quad 6,625$ | 5800 | - | - | - | - | 4,930 |
| 11/4" TimberStrand ${ }^{\text {® }}$ LSL | $7,830^{(2)}$ | 7,250 | 6,290 | 5,365 | 4,580 | 3,930 | 5,450 |
| 1112" TimberStrand ${ }^{\otimes}$ LSL | 9,395 |  | 9,250 | 8,325 | 7,350 | 6,440 | 6,555 |

(1) Capacity is based on calculation.
(2) Capacity is limited to a maximum of 522 psi in accordance with ASTM D7672.

- Values may not be increased for duration of load.



## Fastener Spacing for TJI® Joists

|  | Closest On-Centre Spacing per Row ${ }^{(1)}$ |  |  |
| :---: | :---: | :---: | :---: |
| TJI® |  |  | 16d (0.162" x 312") |
| 110 and 210 | $4{ }^{4}$ | $4^{\text {"(2) }}$ | $6{ }^{\prime \prime}$ |
| 230 | $4 "$ | $4^{\prime \prime}(2)$ | $6 "$ |
| 360, 560 and 560D | 3" | $4^{\prime \prime}(2)$ | $6{ }^{\prime \prime}$ |

(1) Stagger nails when using $4^{4}$ on-centre spacing or less and maintain $3 / 8^{"}$ joist and panel edge distance. One row of fasteners is permitted (two at abutting panel edges) for diaphragms. For other applications, multiple rows of fasteners are permitted if the rows are offset at least $1 / 2^{\prime \prime}$ and staggered.
(2) Can be reduced to $3^{\prime \prime}$ on-centre for light gauge steel straps with $10 \mathrm{~d}\left(0.148^{\prime \prime} \times 1 / 2^{\prime \prime}\right)$ nails.
" Maximum spacing of nails is 18 " on-centre for joists $\leq 16$ " deep; 24 " on-centre for joists > 16 " deep.

- 14 gauge staples may be substituted for $8 \mathrm{~d}\left(0.113^{\prime \prime} \times 2^{1} / 2^{\prime \prime}\right)$ nails if minimum penetration of 1 " is achieved.
- Table also applies to the attachment of TJ®® rim joists and blocking panels to the wall plate.


## Nails Installed on the Narrow Face

| Nail Size | Closest On-Center Spacing per Row |  |  |
| :---: | :---: | :---: | :---: |
|  | 11/8" TJ® Rim Board ${ }^{(1)}$ | TimberStrand ${ }^{\text {® }}$ LSL |  |
|  |  | $11 / 4$ " | $11 / 2^{\prime \prime}$ |
| $\begin{gathered} \text { 8d (0.113" or 0.131" x } 21 / 2 "), \\ 10 \mathrm{~d}\left(0.128^{\prime \prime} \times 3^{\prime \prime}\right), 12 \mathrm{~d}\left(0.128^{\prime \prime} \times 31 / 4^{\prime \prime}\right) \end{gathered}$ | $6{ }^{\prime \prime}$ | $4 "$ | $3{ }^{\prime \prime}$ |
| 10d (0.148" $\times 3$ "), 12d (0.148" x 31/4") | $6{ }^{\prime \prime}$ | $4 "$ | $3{ }^{\prime \prime}$ |
| $16 \mathrm{~d}\left(0.162^{\prime \prime} \times 31 / 22^{\prime \prime}\right)$ | $16^{\prime \prime}(2)$ | $6^{\prime \prime}(3)$ | $6^{\prime \prime}(3)$ |
| (0.131" x 3"-31/2") | $6^{\prime \prime}$ | $4{ }^{\prime \prime}$ | $3^{\prime \prime}$ |

(1) $11 / 8^{\prime \prime} \mathrm{TJ} \oplus$ Rim Board is allowed with joist depths $\leq 16^{\text {" }}$ only.
(2) Can be reduced to $5^{\prime \prime}$ on-centre if nail penetration into the narrow edge is no more than $1^{11 / 4 "}$ (to minimize splitting).
(3) Can be reduced to 4 " on-centre if nail penetration into the narrow edge is no more than $11 / 4$ " (to minimize splitting).

- To minimize splitting, maintain edge distance and row spacing of $21 / 2 x$ nail diameter or $3 / 8^{\prime \prime}$, whichever is greater. Multiple rows must be staggered and equally spaced from the centreline of the narrow face axis.
- 14 gauge staples may be substituted for $8 \mathrm{~d}\left(0.113^{\prime \prime} \times 21 / 2\right.$ ") nails if minimum penetration of $1^{1 "}$ is achieved.

Also see nailing requirements on page 25.

Backer block: Install tight to top flange (tight to bottom flange with face mount hangers). Attach per table below


With top mount hangers, backer block required only for factored downward loads exceeding 395 lbs or for uplift conditions

## Filler and Backer Block Sizes

| $\mathrm{TJ}{ }^{\circledR}$ |  | 110 |  | 210 |  | 230 or 360 |  | 360 | 560 |  |  | 560D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $91 / 22^{\prime \prime}$ or $117 / 8^{\prime \prime}$ | $14 "$ | 91/2" or $117 / 8^{\prime \prime}$ | $14^{\prime \prime}$ or 16" | $91 / 2$ or $111 / 8{ }^{\text {" }}$ | $14^{\prime \prime}$ or 16" | 18 " or 20" | 91/2" or 111/8" | $14^{\prime \prime}$ or 16" | 18 " or 20" | $22^{\prime \prime}$ or 24" |
| Filler Blo (Detail | ck ${ }^{(1)}$ | 2x6 | 2x8 | $\begin{aligned} & 2 \times 6+3 / 810 \\ & \text { sheathing } \end{aligned}$ | $\begin{aligned} & 2 \times 8+3 / 8^{\prime \prime} \\ & \text { sheathing } \end{aligned}$ | $\begin{aligned} & 2 \times 6+1 / 21^{1 \prime} \\ & \text { sheathing } \end{aligned}$ | $\begin{aligned} & 2 \times 8+1 / 2^{11} \\ & \text { sheathing } \end{aligned}$ | $\begin{aligned} & 2 \times 12+1 / 2 " 1 \\ & \text { sheathing } \end{aligned}$ | $\begin{aligned} & \text { Two } \\ & 2 \times 6 \end{aligned}$ | $\begin{aligned} & \text { Two } \\ & 2 \times 8 \end{aligned}$ | $\begin{aligned} & \text { Two } \\ & 2 \times 12 \end{aligned}$ | Four $3 / 4^{\prime \prime} \times 15^{\prime \prime}$ sheathing |
| Cantilever Filler (Detail E4) |  | $\begin{gathered} 2 \times 6 \\ 4^{\prime}-0^{\prime \prime} \text { long } \end{gathered}$ | $\left\lvert\, \begin{gathered} 2 \times 10 \\ 6^{\prime}-0^{\prime \prime} \text { long } \end{gathered}\right.$ | $\begin{aligned} & 2 \times 6+3 / 8^{\prime \prime} \\ & \text { sheathing, } \\ & 4^{\prime}-0^{\prime \prime} \text { long } \end{aligned}$ | $\begin{aligned} & 2 \times 10+3 / 8^{\prime \prime} \\ & \text { sheathing, } \\ & 6^{\prime}-0^{\prime \prime} \text { long } \end{aligned}$ | $\begin{aligned} & 2 \times 6+1 / 2 " 1 \\ & \text { sheathing, } \\ & 4^{\prime}-0^{" 1} \text { long } \end{aligned}$ | $\begin{aligned} & 2 \times 10+1 / 2 " \\ & \text { sheathing, } \\ & 6^{\prime}-0^{\prime \prime} \text { long } \end{aligned}$ | Not applicable | Not applicable |  |  |  |
| Backer Block ${ }^{(1)}$ (Detail F1 or H2) |  | $5 / 8^{\prime \prime}$ or $3 / 4{ }^{\prime \prime}$ |  | $3 / 4$ " or 7/8" |  | $7 / 8$ " or 1" net |  |  | $2 \times 6$ | 2x8 | $2 \times 12$ | Two 3/4" $\times 15^{\prime \prime}$ sheathing |
| Nail Size | Filler | (0.131" $\times$ 3") |  |  |  |  |  |  |  |  | 131 " $\times 31 / 2$ ") |  |
|  | Backer |  |  |  |  |  |  |  |  |  | (131" x 3") |  |
| Nail | Filler ${ }^{(3)}$ |  |  |  | 15 |  |  |  |  | 32 |  | 50 |
| Quantity ${ }^{(2)}$ | Backer |  |  |  | 15 |  |  |  |  | 15 |  | 15 |

(1) If necessary, increase filler and backer block height for face mount hangers and maintain $1 / 8$ " gap at top of joist. See detail W. Filler and backer block dimensions should accommodate required nailing without splitting. The suggested minimum length is 24 " for filler and 12 " for backer blocks.
(2) Clinch nails when possible.
(3) For filler block connections, drive nails from alternating sides.

Web Stiffener Attachment


Web Stiffener Requirements

| TJ ${ }^{\text {® }}$ | Depth (in.) | Minimum Web Stiffener Size | Nail Type | Quantity |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | End | Int. |
| 110 | All | $5 / 8^{\prime \prime} \times 25 / 16^{\prime \prime}(1)$ | 8d (0.113" x 2½) | 3 | 3 |
| 210 | All | $3 / 44^{11} \times 25 / 16^{\prime \prime}(1)$ |  | 3 | 3 |
| 230,360 | All | $7 / 81 \times 25 / 16^{\prime \prime}(1)$ |  | 3 | 3 |
| 560 | All | $2 \times 4{ }^{(2)}$ | 16d (0.135" x 312") | 3 | 3 |
| 560D | 22" | $2 \times 4{ }^{(2)}$ | 16 d (0.135" $\times 31 / 2 \mathrm{~L}$ ) | 6 | 11 |
|  | 24" |  |  | 6 | 13 |

(1) CSA standards 0151,0325 , or 0437 with face grain vertical.
(2) Construction grade or better.

Also see nailing requirements on page 25.


TJI® Joist Nailing Requirements at Bearing (Maximum slope for $18^{\text {" }}$-24" joists is $3: 12$ )
End Bearing
$\left(13 / 4^{\prime \prime}\right.$ minimum bearing required)

## TJI Joist to Bearing Plate

## connector is required.

( $31 / 2^{\prime \prime}$ minimum bearing required)


Slopes 3:12 or less:
One 8d ( $0.113^{\prime \prime} \times 21 / 22^{2}$ ) nail each side. Use ( 0.131 " x $3^{\prime \prime}$ ) . See detail R7.

Slopes greater than 3:12 (for depths $\leq 16$ " only):

When slope exceeds $1 / 4$ : 12 for a $2 \times 4$ wall or $1 / 8: 12$ for a

Blocking to Bearing Plate
$11 / 8^{\prime \prime} \mathrm{TJ}$ ® Rim Board (with depths $\leq 16^{\prime \prime}$ ) $11 / 4^{\prime \prime}$ or $1 \frac{1}{2}$ " TimberStrand ${ }^{\circledR}$ LSL: TJ® joist blocking: ( $0.131^{\prime \prime} \times 3^{\prime \prime}$ ) nails at $6^{\prime \prime}$ on-centre
Shear transfer nailing: nail schedule

## These Conditions Are NOT Permitted:



DO NOT cut holes too close to support.

Refer to Allowable Holes on pages 16 and 24 for minimum distance from support.


DO NOT bevel cut joist beyond inside face of wall.


DO NOT overhang birdsmouth cut from inside face of plate.
TJ』® joist flange must bear fully on the plate. See detail BC on page 31.



R7 $\mathrm{RH}_{\mathrm{W}}^{\mathrm{R}} \mathrm{S}_{\mathrm{S}}^{\mathrm{R}}$ RTS is allowed only with joist depths $\leq 16^{\prime \prime}$.

R9


R8


## $R 10$ R10

## Shear Blocking and Ventilation Holes (Roof Only)



For TJ』® joists with slopes of $10: 12$ to 12:12, the vertical depth of the shear blocking at bearing will require $11 / 8^{\prime \prime} T J^{\circledR}$ Rim Board, 11/4" or 11/2" TimberStrand ${ }^{\circledR}$ LSL that is one size deeper than the $\mathrm{TJ}{ }^{\circledR}$ joist. DO NOT use $11 / 8^{\prime \prime} \mathrm{T} \Theta^{\circledR}$ Rim Board with $18^{\prime \prime}-24^{\prime \prime} \mathrm{TJ}{ }^{\circledR}$ joists or in ventilation-hole applications.


LSTA24 (Simpson or USP) strap with twelve 10d (0.148" x
$11 / 2^{\prime \prime}$ ) nails required at H5S with slopes greater than 3:12


H5 H5S Detail H5S is allowed only with joist depths $\leq 16^{\prime \prime}$.

Beveled Plate Requirements


| Required Bearing <br> Length | Maximum Slope <br> Without Beveled Plate |
| :---: | :---: |
| $13 / 4^{\prime \prime}$ | $1 / 2: 12$ |
| $31 / 1^{\prime \prime}$ | $1 / 4: 12$ |
| $51 / 2^{\prime \prime}$ | $1 / 8: 12$ |



Variable slope joist hanger. See pages 14-15 and 22-23. Beveled web stiffener required both sides.

H6 H6S Detail H6S is allowed only with joist depths $\leq 16^{\prime \prime}$.

## Filler and Backer Block Sizes

| $\frac{\mathrm{TJI®}}{\text { Depth }}$ |  | 110 |  | 210 |  | 230 or 360 |  | 360 | 560 |  |  | 560D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $91 / 2$ or $111 / 8^{\prime \prime}$ | 14" | 91/2" or $111 / 8{ }^{\text {" }}$ | $14^{\prime \prime}$ or 16" | $91 / 2^{\prime \prime}$ or $111 / 8^{\prime \prime}$ | $14^{\prime \prime}$ or 16" | 18 " or 20" | $91 / 2^{\prime \prime}$ or $111 / 8^{\prime \prime}$ | $14^{\prime \prime}$ or 16" | 18 " or 20" | $22^{\prime \prime}$ or 24" |
| Filler Blo (Detail |  | 2x6 | 2x8 | $2 \times 6+3 / 8 "$ <br> sheathing | $2 \times 8+3 / 8 "$ sheathing | $2 \times 6+1 / 21$ sheathing | $\begin{aligned} & 2 \times 8+1 / 21 \\ & \text { sheathing } \end{aligned}$ | $\begin{array}{\|c\|} \hline 2 \times 12+1 / 2 " \\ \text { sheathing } \end{array}$ | $\begin{aligned} & \text { Two } \\ & 2 \times 6 \end{aligned}$ | $\begin{aligned} & \text { Two } \\ & 2 \times 8 \end{aligned}$ | $\begin{aligned} & \hline \text { Two } \\ & 2 \times 12 \end{aligned}$ | Four $34^{11} \times 15^{11}$ sheathing |
| Cantilever Filler (Detail E4) |  | $\begin{gathered} 2 \times 6 \\ 4^{\prime}-0^{\prime \prime} \text { long } \end{gathered}$ | $\left\|\begin{array}{c} 2 \times 10 \\ 6^{\prime}-0^{\prime \prime} \text { long } \end{array}\right\|$ | $\begin{aligned} & 2 \times 6+3 / 8^{\prime \prime} \\ & \text { sheathing, } \\ & 4^{\prime}-0^{\prime \prime} \text { long } \end{aligned}$ | $\begin{aligned} & 2 \times 10+3 / 8 " \\ & \text { sheathing, } \\ & 6^{\prime}-0^{\prime \prime} \text { long } \end{aligned}$ | $\begin{aligned} & 2 \times 6+1 / 2 " \\ & \text { sheathing, } \\ & 4^{4}-0^{\prime \prime} \text { long } \end{aligned}$ | $\begin{aligned} & 2 \times 10+1 / \text { "'" }^{\prime} \\ & \text { sheathing, } \\ & 6^{\prime}-0^{\prime \prime} \text { long } \end{aligned}$ | Not applicable | Not applicable |  |  |  |
| Backer Block ${ }^{(1)}$ (Detail F1 or H2) |  | $5 / 8{ }^{\text {" }}$ or 3/4" |  | $3 / 4$ or 7/8" |  | $7 / 8$ " or 1" net |  |  | 2x6 | 2x8 | $2 \times 12$ | Two 3/4" $\times 15^{\prime \prime}$ sheathing |
| Nail Size | Filler | (0.131" $\times 3$ ") |  |  |  |  |  |  |  |  | $\left.131{ }^{11} \times 1 \times 122^{\prime \prime}\right)$ |  |
|  | Backer |  |  |  |  |  |  |  |  |  | .131" x 3") |  |
| Nail | Filler ${ }^{(3)}$ |  |  |  | 15 |  |  |  |  | 32 |  | 50 |
| Quantity ${ }^{(2)}$ | Backer |  |  |  | 15 |  |  |  |  | 15 |  | 15 |

(1) If necessary, increase filler and backer block height for face mount hangers and maintain $1 / 8$ " gap at top of joist. See detail W. Filler and backer block dimensions should accommodate required nailing without splitting. The suggested minimum length is 24 " for filler and 12 " for backer blocks.
(2) Clinch nails when possible.
(3) For filler block connections, drive nails from alternating sides.


## Slope Factors

| Slope | $21 / 2: 12$ | $3: 12$ | $31 / 2: 12$ | $4: 12$ | $41 / 2: 12$ | $5: 12$ | $6: 12$ | $7: 12$ | $8: 12$ | $9: 12$ | $10: 12$ | $11: 12$ | $12: 12$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Factor | 1.021 | 1.031 | 1.042 | 1.054 | 1.068 | 1.083 | 1.118 | 1.158 | 1.202 | 1.250 | 1.302 | 1.357 | 1.414 |

## MATERIAL WEIGHTS AND CONVERSION TABLES

## Material Weights

(Include $\mathrm{TJ}{ }^{\circledR}$ weights in dead load calculations-see Design Properties tables on pages 6 and 17 for joist weights)

## Floor Panels

| Southern Pine |  |
| :---: | :---: |
| 1/2" plywood | 1.7 psf |
| 5/8" plywood | 2.0 psf |
| 3/4" plywood | 2.5 psf |
| 11/8" plywood | 3.8 psf |
| 1/2" OSB | 1.8 psf |
| 5/8" OSB | 2.2 psf |
| 3/4" OSB | 2.7 psf |
| 7/8" OSB | 3.1 psf |
| 11/8" OSB | 4.1 psf |
| Based on: Southern pine - 40 pcf for plywood, 44 pcf for OSB |  |
| Roofing |  |
| Asphalt shingles | 2.5 psf |
| Wood shingles | 2.0 psf |
| Clay tile | 14.0 psf |
| Slate ( $3 / 8{ }^{\prime \prime}$ thick). | 15.0 psf |

## PSF to PLF

| O.C. <br> Spacing | Load in Pounds Per Square Foot (PSF) |  |  |  |  |  |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: |
|  | $\mathbf{2 0}$ | $\mathbf{2 5}$ | $\mathbf{3 0}$ | $\mathbf{3 5}$ | $\mathbf{4 0}$ | $\mathbf{4 5}$ | $\mathbf{5 0}$ | $\mathbf{5 5}$ | $\mathbf{6 0}$ |  |  |
|  | Load in Pounds Per Linear Foot (PLF) |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{1 2}$ | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 |  |  |
| $\mathbf{1 6 "}$ | 27 | 34 | 40 | 47 | 54 | 60 | 67 | 74 | 80 |  |  |
| $\mathbf{1 9 . 2}$ | 32 | 40 | 48 | 56 | 64 | 72 | 80 | 88 | 96 |  |  |
| $\mathbf{2 4}$ | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 | 120 |  |  |

## Roll or Batt Insulation (1" thick):

Rock wool. ..... 0.2 psf
Glass wool ..... 0.1 psf
Floor Finishes
Hardwood (nominal 1") ..... 4.0 psf
Sheet vinyl ..... 0.5 psf
Carpet and pad ..... 1.0 psf
$3 / 4$ " ceramic or quarry tile ..... 10.0 psf
Concrete:
Regular (1") ..... 12.0 psf
Lightweight (1"). ..... 8.0 to 10.0 psf
Gypsum concrete (3/4") ..... 6.5 psf
Ceilings
Acoustical fibre tile ..... 1.0 psf
1/2" gypsum board. ..... 2.2 psf
5/8" gypsum board ..... 2.8 psf
Plaster (1" thick) ..... 8.0 psf

## Metric to Imperial

| Metric Unit | Imperial Conversion |
| :---: | :---: |
| 1 kN | 0.2248 kip |
| $1 \mathbf{~ N}$ | 0.2248 lb |
| 1 m | 3.281 ft |
| 1 mm | 0.0394 in. |
| 1 kg | 2.205 lb mass |
| $1 \mathrm{~N} \cdot \mathrm{~m}$ | $0.7376 \mathrm{lb} \cdot \mathrm{ft}$ |
| $1 \mathrm{~N} \cdot \mathrm{~m}$ | $8.851 \mathrm{lb} \cdot \mathrm{in}$. |
| $1 \mathrm{~mm}^{4}$ | $2.402 \times 10^{-6} \mathrm{in} .^{4}$ |
| 1 Pa | $0.0209 \mathrm{lb} / \mathrm{ft}^{2}$ |
| 1 kPa | $0.1450 \mathrm{lb} / \mathrm{in} .^{2}$ |

## Imperial to Metric

| Imperial Unit | Metric Conversion |
| :---: | :---: |
| 1 kip | 4.448 kN |
| 1 lb | 4.448 N |
| 1 ft | 0.3048 m |
| 1 in. | 25.40 mm |
| 1 lb mass | 0.4536 kg |
| $1 \mathrm{lb} \cdot \mathrm{ft}$ | $1.356 \mathrm{~N} \cdot \mathrm{~m}$ |
| $1 \mathrm{lb} \cdot \mathrm{in}$. | $0.1130 \mathrm{~N} \cdot \mathrm{~m}$ |
| $1 \mathrm{in} .^{4}$ | $0.4162 \times 10^{6} \mathrm{~mm}^{4}$ |
| $1 \mathrm{lb} / \mathrm{ft}^{2}$ | 47.88 Pa |
| $1 \mathrm{lb} / \mathrm{in} .^{2}$ | 6.895 kPa |

## NOTES

## WE CAN HELP YOU BUILD SMARTER

You want to build solid and durable structures-we want to help. Weyerhaeuser provides high-quality building products and unparalleled technical and field assistance to support you and your project from start to finish.

Floors and Roofs: Start with the best framing components in the industry: our Trus Joist ${ }^{\circledR}$ TJI ${ }^{\circledR}$ joists; TimberStrand ${ }^{\circledR}$ LSL rim board; and TimberStrand ${ }^{\circledR}$ LSL, Microllam ${ }^{\circledR}$ LVL, and Parallam ${ }^{\circledR}$ PSL headers and beams. Pull them all together with our self-gapping and self-draining Weyerhaeuser Edge Gold ${ }^{\text {TM }}$ floor panels and durable Weyerhaeuser roof sheathing.

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 two-way nail lines.

Software Solutions: Whether you are a design professional or lumber dealer, Weyerhaeuser offers an array of software packages to help you specify individual framing members, create cut lists, manage inventories-even help you design a complete structural frame. Contact your Weyerhaeuser representative to find out how to get the software you need.

Technical Support: Need technical help? Weyerhaeuser has one of the largest networks of engineers and sales representatives in the business. Call us for help, and a skilled member from our team of experts will answer your questions and work with you to develop solutions that meet all your structural framing needs.

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[^0]:    * Weyerhaeuser recommends using a subfloor adhesive that has been qualified as a Class 1/8 in., Type P/0 subfloor adhesive in accordance with ASTM D3498-19.

[^1]:    Let one of our experienced Territory Managers perform a TJ-Pro Rating assessment on your floors to give you insight on how well your floors will perform against your customers expectations. They can also help recommend products which will give you the optimal results you are looking for without overspending.

